

Emnemodul: Advanced Process Control

21 Nov. 2023. Time: 1000 – 1300.

Answer as carefully as possible, preferably using the available space. There are in total 5 questions. Answer all questions in English.

No printed or hand-written support material is allowed. A specific basic calculator is allowed.

Problem 1 – General questions (20%)

- a) What are the main approaches for decomposing the control system into smaller elements? Make a figure (block diagram) to illustrate the decomposition.
- b) What are the main objectives of the supervisory control layer?
- c) What are the main objectives of the basic (stabilizing) control layer?
- d) Explain the main ideas behind self-optimizing control, RTO and extremum seeking control. How can these three strategies be combined?
- e) What is back-off and when is it used? When is it important to minimize back-off?
- f) What is a typical cost function in the RTO layer?
- g) What is the difference between economic MPC and setpoint-based MPC? What is a typical cost function in the two cases?
- h) The “pair-close” rule is the most important rule for choosing pairings for decentralized control. Assume that you have $G(s) = k e^{-\theta s} / (\tau s + 1)$. What values does this rule imply that you would like to have for each of the three parameters k , θ and τ (large, no effect or small)?
- i) What is the “input saturation pairing rule”? When should it be used? If it is satisfied, what does it imply in terms of MV-CV switching? Give an example.

Problem 2 – Optimal process operation (20%)

Consider a simple steady-state process (fast dynamics) with one unconstrained degree of freedom and two disturbances. The cost function to be minimized during operation is

$$J = (u - 2d_1)^2 + (u - 2d_2)^2$$

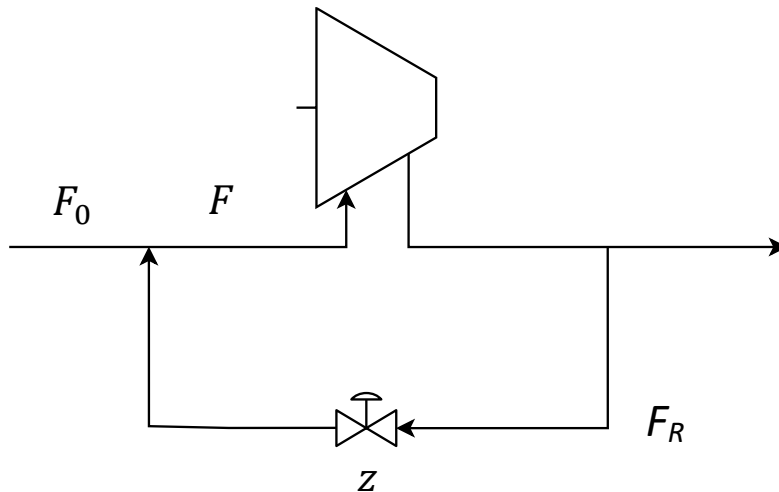
Nominally we have $d_1 = d_2 = 0$, and the expected magnitudes of the disturbances are $|d_1| \leq 1$ and $|d_2| \leq 1$. We have available three measurements.

$$y_1 = u + 0.1 d_1, \quad y_2 = 0.1u - d_2, \quad y_3 = d_1 + d_2$$

- (a) Use the nullspace method to find the self-optimizing $c = Hy$ which when kept constant gives zero loss for the expected disturbances (at least locally and with perfect measurements). What is the optimal setpoint for c ?
- (b) Explain how to find the optimal H if we include measurements noise of magnitude $|n_{yi}| \leq 0.2$ for each of the three measurements. (Give the formula for H and give the matrices G^y and Y needed to compute H). What is this method called? Finding the final H is maybe a bit too much for hand calculations as it involves a matrix inversion; how large is the matrix to be inverted in this case?

Problem 3 – Compressor with constraints (15%)

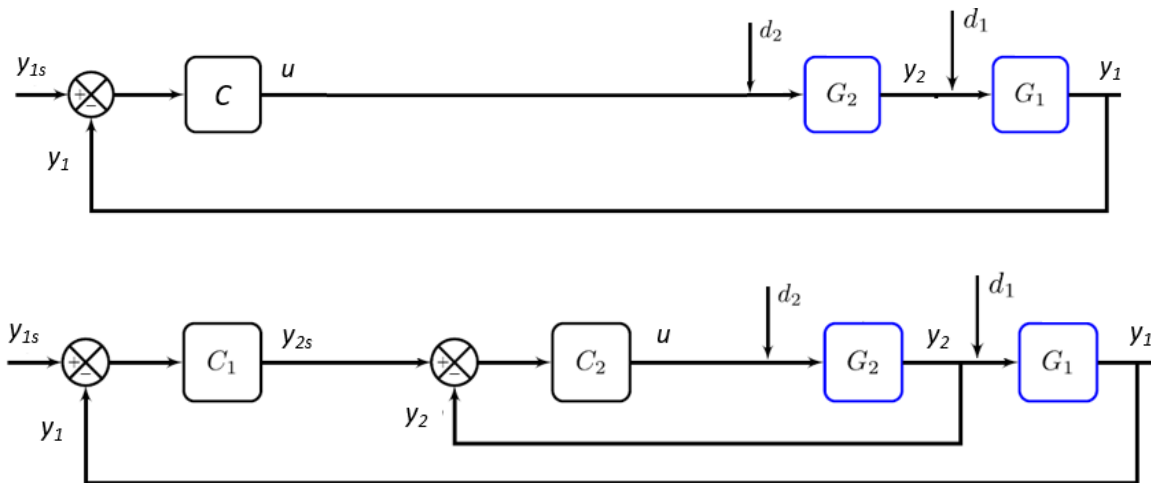
Consider a constant-speed compressor (which means that it has no degrees of freedom for control) with an adjustable recycle F_R which should be minimized whenever possible. The following constraints need to be satisfied: $F \geq F_{min}$, $F_0 \leq F_{0,max}$, $z \geq 0$, $z \leq 1$. The first constraint is to avoid compressor surge; the second constraint is because the compressor is feeding a reactor and too high flowrates are bad for the catalyst.



- (a) To switch between active constraints we want to use selectors. Give the three selector rules (Rule 1 is about min- or max- selector, Rule 2 is about order of selectors, Rule 3 is about valve constraints).
- (b) Use the selector rules to propose a control system. You may add flow sensors as needed.

Problem 4 – Cascade control and tuning (25%)

Below are shown control schemes for the process $G=G_1G_2$ for the case without and with cascade control.



- (a) What motivates the use of cascade control?
- (b) Derive the transfer function from d_2 to y_1 for the two cases.

In the following let: $G_1 = 3/(18s+1)$, $G_2 = e^{-0.4s}/(s+1)$

- (c) Do you recommend cascade control in this case?
- (d) Suggest “tight” SIMC PI-tunings for C (for the case without cascade).

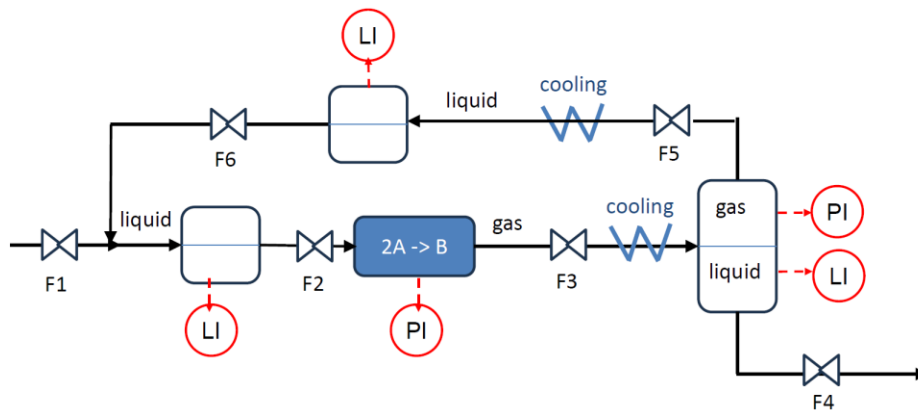
In the rest consider cascade control.

- (e) Suggest “tight” SIMC PI-tunings for the slave controller C_2 .
- (f) Suggest “tight” SIMC PI-tunings for the master controller C_1 .
- (g) It is given that the time scale separation between the slave and master loops should be at least 5. What is the motivation for such a requirement? Is this satisfied for your case? If not suggest how to change the PI tunings.

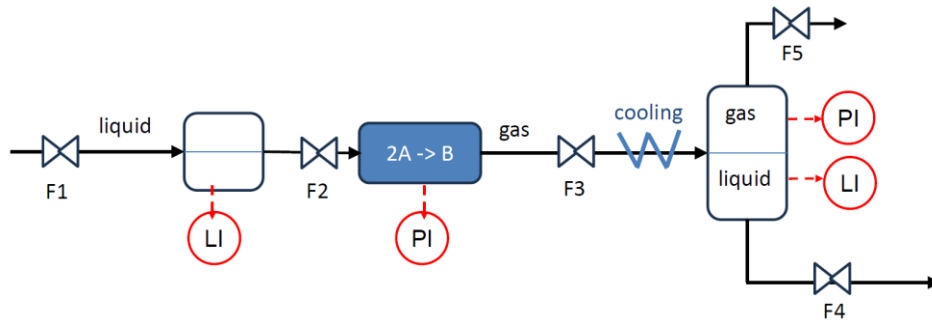
Problem 5 – Inventory control for reactor process (20%)

- (a) Consider the flowsheet below. The reactor is exothermic with a liquid feed and gas product. The feed F1 contains mostly component A and the liquid product F4 contains mostly component B. The gas from the separator is recycled. The pressure (PI) and level (LI) sensors should be used for inventory control.

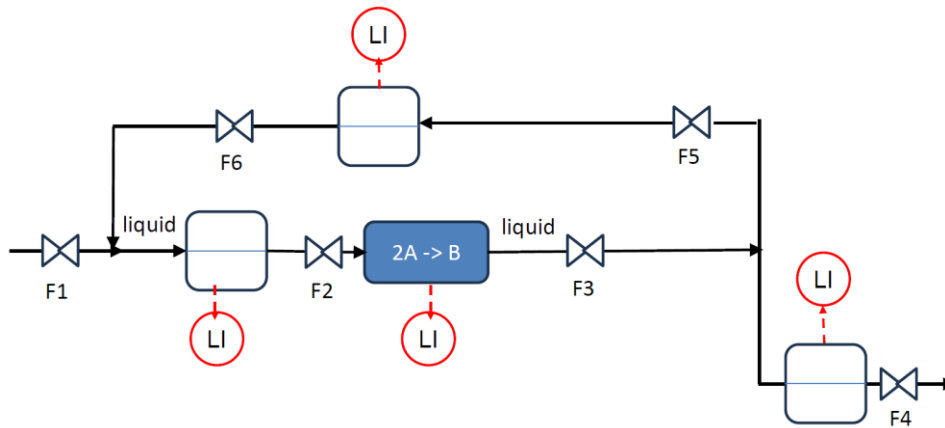
Suggest a control scheme for the case when the feedrate is set (F1 is the TPM).



- (b) Consider a similar process without recycle. Suggest a bidirectional inventory control scheme. What advantages does it have compared to a “fixed” control scheme (similar to the one in part a)?



- (c) Consider a case where the separator is replaced by a split. All flows are liquid in this case. It is given that we should have a given ratio $R = F_6/F_1$. Propose a control scheme for the case where F_4 is given (F_4 is the TPM). You can add extra flow sensors as needed.



Extra sheet

Extra sheet