

Integrated optimization and control

Marius Støre Govatsmark

Department of Chemical Engineering, NTNU

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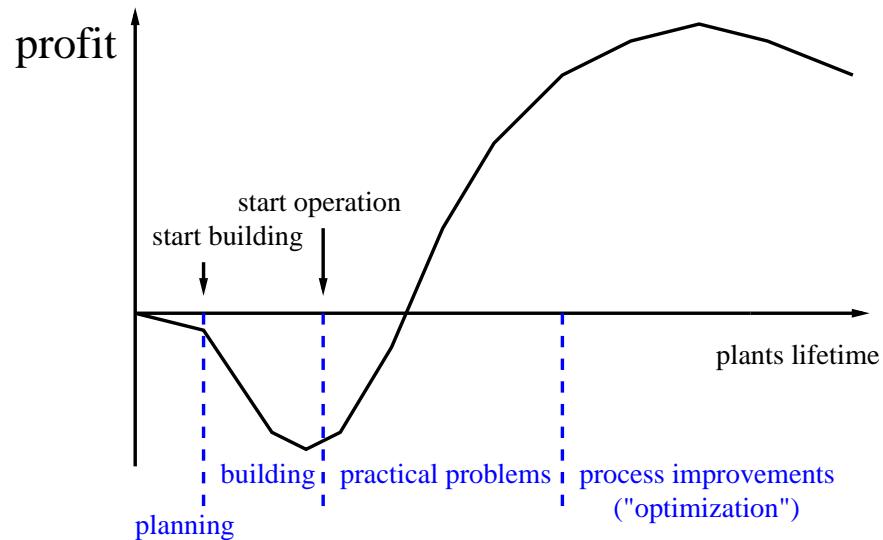
Outline

- Thesis overview
- Selection of controlled variables and setpoints (chap. 2-4)
 - Self-optimizing control
 - Ex 1: Long-distance running
 - Ex 2: Reactor, separator and recycle process
- Plantwide control (chap. 5-6)
- Controllability and distillation column (chap. 7)
- Concluding remarks and further work

Thesis overview

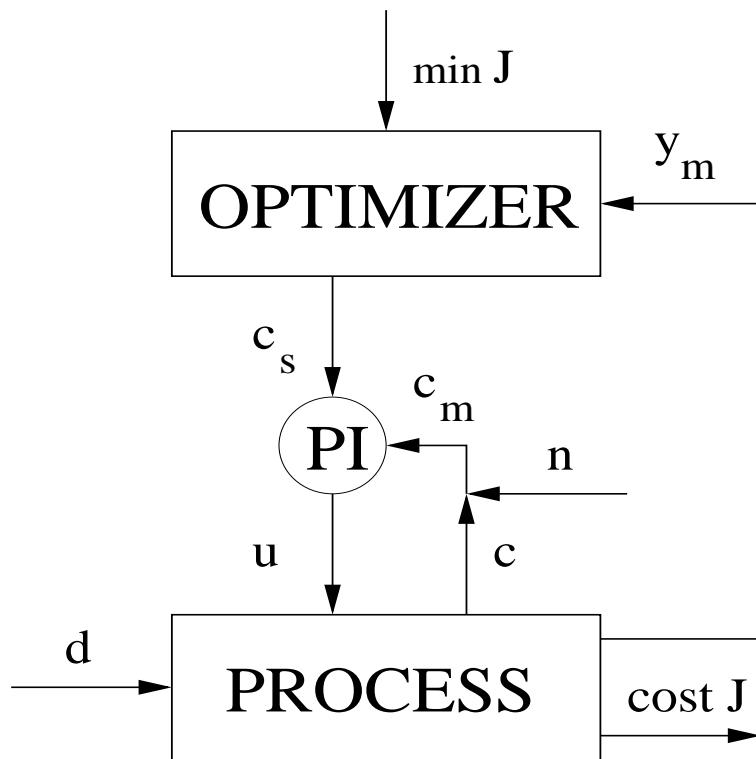
- **Chapter 2:**
Control Structure Selection for Reactor, Separator and Recycle Process
- **Chapter 3:**
Selection of Controlled Variables and Robust Setpoints
- **Chapter 4:**
Control Structure Design for An Evaporation Process
- **Chapter 5:**
Application of a Plantwide Control Design Procedure to a Combined Cycle Power Plant
- **Chapter 6:**
Application of a Plantwide Control Design Procedure to a Distillation Column with Heat Pump
- **Chapter 7:**
Optimal Number of Stages in Distillation with respect to Controllability

Where am I?



- Process industry
- Primary mature phase
- Improving operation ("optimization")

Selection of controlled variables and setpoints (chap. 2-4)



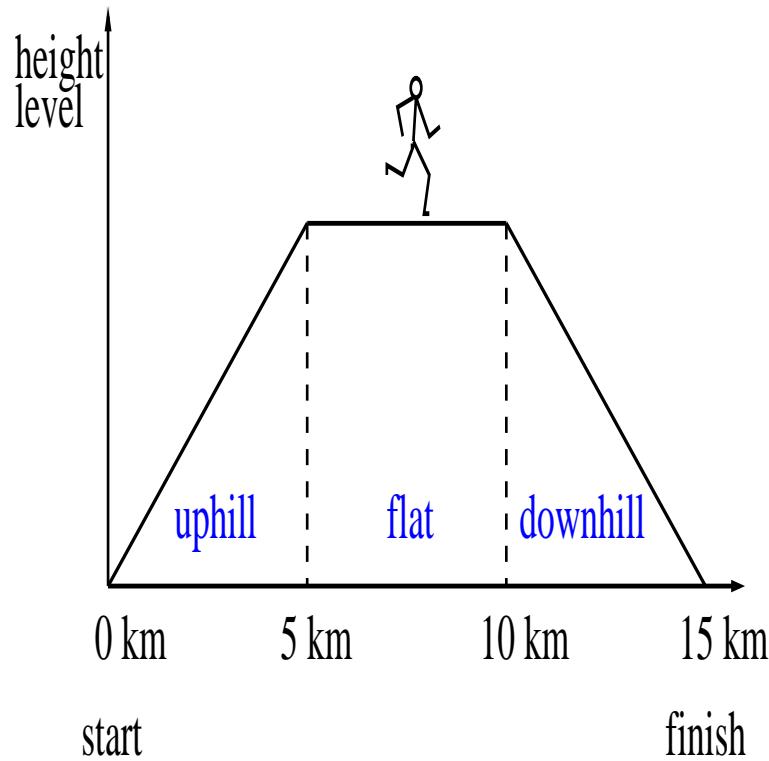
- Which variables? c
- Which setpoints? c_s
(robust optimization)
- Can we achieve acceptable economic operation with constant setpoints
(self-optimizing control)?

$d_c = c - c_s$: implementation error

Mathematical formulation: Best constant setpoint policy

$$\{c(x, u, d), c_s\} = \arg \left\{ \min_{c(u, x, d)} \begin{bmatrix} \min_{x_i, u_i, c_s} \sum_i w_i J(x_i, u_i, d_i) \\ f(x_i, u_i, d_i) = 0 \\ g(x_i, u_i, d_i) \leq 0 \\ c(x_i, u_i, d_i) = c_s + d_{c,i} \\ d_i = d_0 + \Delta d_i \\ d_{c,i} = d_{c,0} + \Delta d_{c,i} \\ \Delta d_i \in D_d, \Delta d_{c,i} \in D_c \end{bmatrix} \right\}$$

Example 1: Long-distance running



Optimal running (operation):
 $u_{opt} = u_{opt}(terraine, energy) \neq u_{max}$

Problem:
Complex model + uncertainties

Manipulated variables:

$$u^T = [\text{speed}]$$

Steady-state degrees of freedom: 1

Minimize time consume

$$J = t_{consumed}$$

Constraints:

$$u \leq u_{max}(terraine, energy)$$

Disturbances (uncertainty):

$$d^T = [\text{terraine energy}]$$

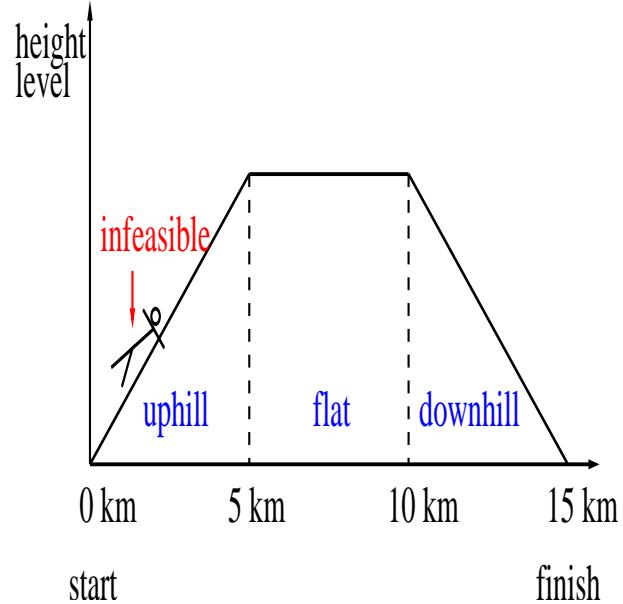
$$\text{terraine} = \{\text{uphill, flat, downhill}\}$$

Candidate controlled variables:

$$c^T = [\text{speed heart - frequency}]$$

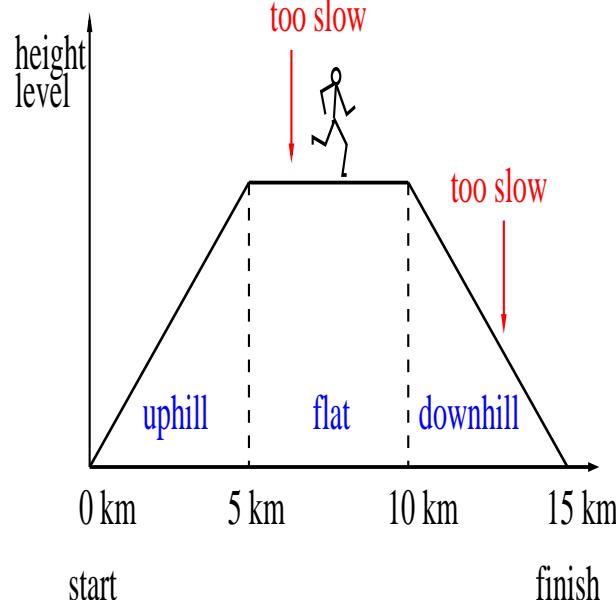
Controlled variable: Speed ($c=u$)

Nominal speed
($c_s = u_{flat}$)



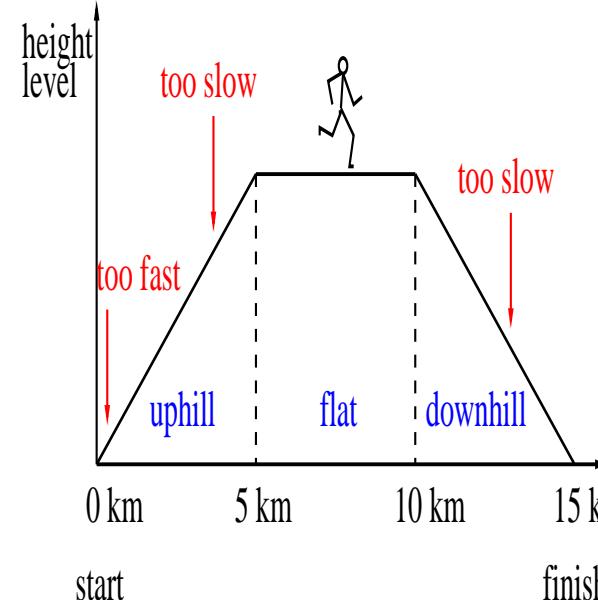
Infeasible

Robust speed
($c_s = u_{uphill}$)



Feasible

Flexible speed
($c_s = u_{flat}$)

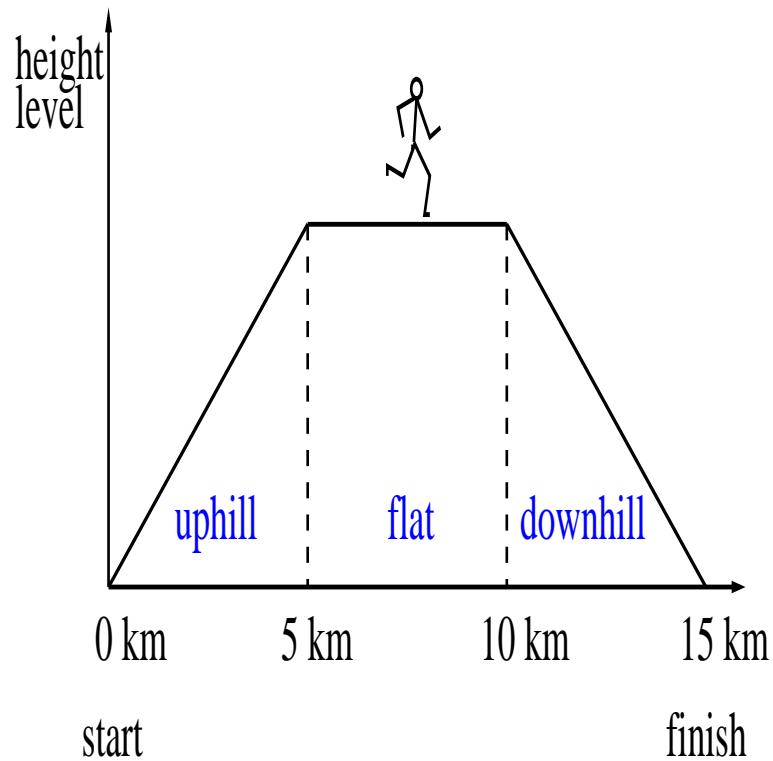


Feasible

Controlled variable: Heart frequency ($c=f$)

Nominal heart frequency

$$(c_s = f_{flat})$$

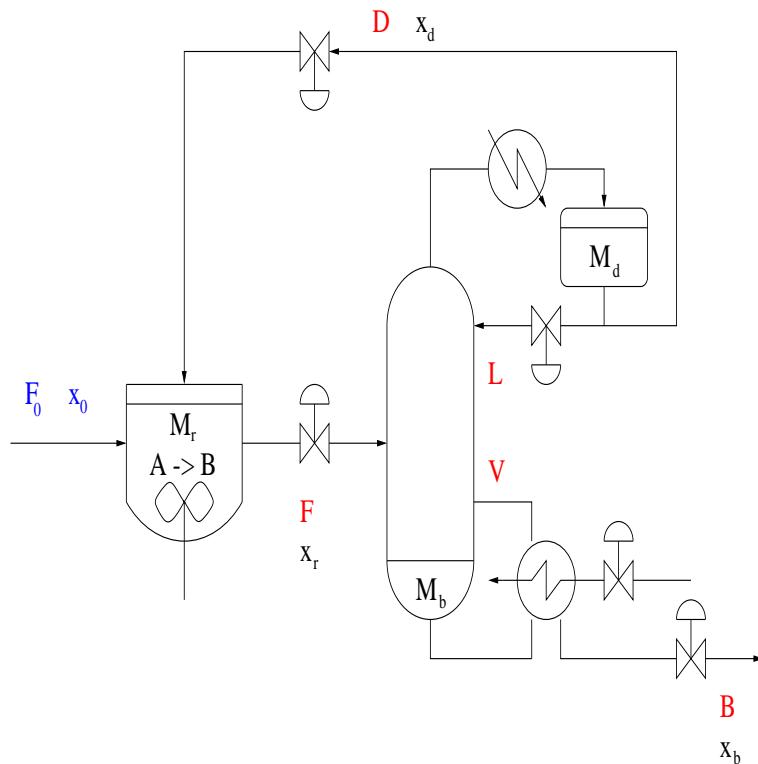


Feasible + close to optimal

$$(u \approx u_{opt}(terraine, distance))$$

Self-optimizing control

Example 2: Reactor-Distillation-Recycle System (Papadourakis, 1987)



Manipulated variables:

$$u^T = [V \ L \ B \ D \ F]$$

Steady-state degrees of freedom: 3

Minimize costs

$$J = V$$

Constraints:

$$x_b \leq 0.015 \frac{\text{molA}}{\text{mol}} \quad \text{active}$$

$$M_r \leq 2800 \text{ kmol} \quad \text{active}$$

$$V \leq 5000 \text{ kmol/h}$$

$$\text{Flows} \geq 0 \text{ kmol/h}$$

Disturbances:

$$d^T = [F_0 \ x_0] = [460 \pm 92 \frac{\text{kmol}}{\text{h}} \ 0.90 \pm 0.05 \frac{\text{m}}{\text{r}}]$$

Procedure for selecting controlled variables (self-optimizing control)

Step 1. Initial system analysis

- Economic objective and constraints
- Degrees of freedom
- Disturbances

Step 2. Identify candidate controlled variable sets

- Use active constraint control
- Initial screening: Minimum singular value
- Process insight

Step 3. Lossevaluation for controlled variable sets, with:

- a. Constant nominal setpoints
- b. Constant robust setpoints
- c. Nominal setpoints with online feasibility correction
(flexible setpoints)

Step 4. Final evaluation and selection of control structure

Step 2: Identify candidate controlled variables

Candidate controlled variables (20):

$$c^T = [L \ V \ D \ B \ F \ M_r \ x_r \ x_B \ x_D \ \frac{L}{F} \ \frac{V}{F} \ \frac{B}{F} \ \frac{D}{F} \ \frac{V}{L} \ \frac{B}{L} \ \frac{D}{L} \ \frac{B}{V} \ \frac{D}{V} \ \frac{B}{D} \ \frac{F}{F_0}]$$

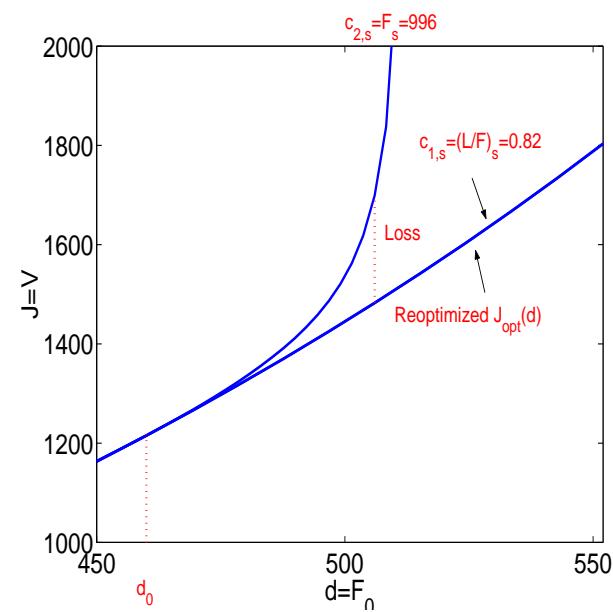
Active constraint control

- Product composition (x_B)
- Reactor holdup (M_r)

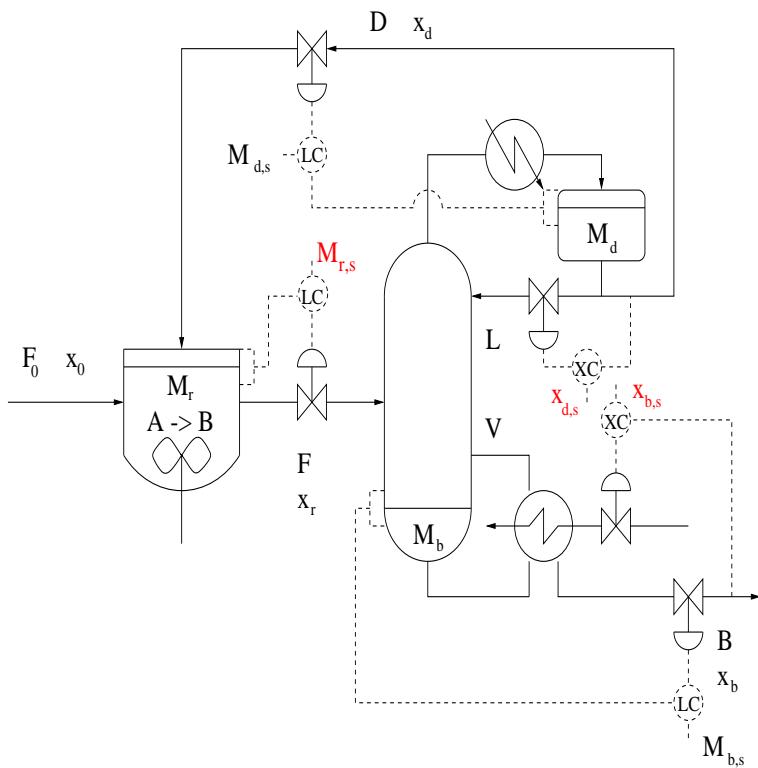
Unconstrained degree of freedom: 1

Step 3a: Loss evaluation with constant nominal setpoints

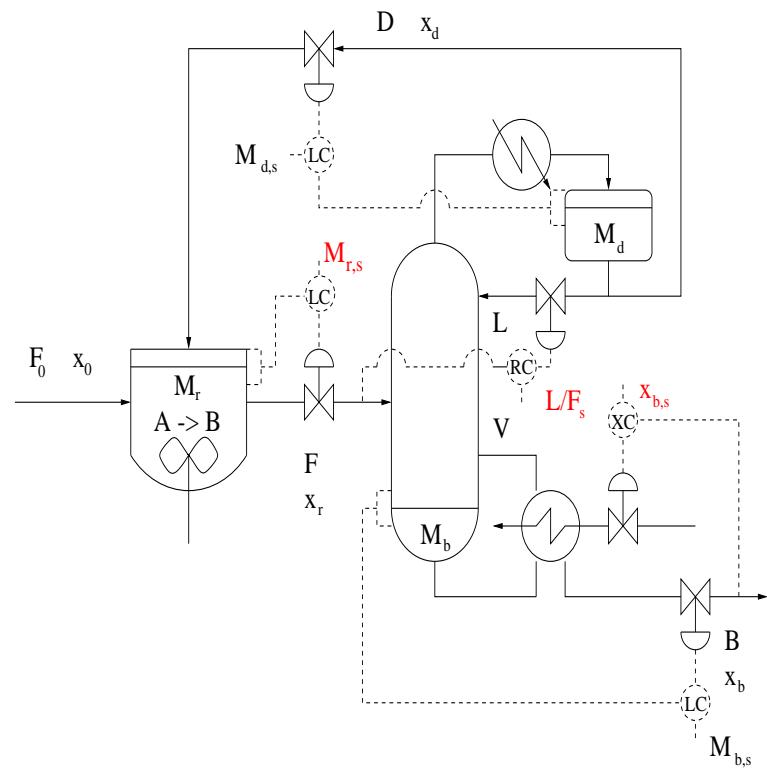
c_1, c_2, c_3		Nominal setpoints		
	$c_{3,s}$	$L_w(\%)$	$L_{max}(\%)$	
Reoptimized	$c_{opt}^*(d)$	5.16	11.03	
x_B, M_r, x_D	0.825	5.22	11.04	
$x_B, M_r, L/F$	0.871	5.39	11.24	
$x_B, M_r, D/L$	0.600	5.40	11.15	
$x_B, M_r, D/V$	0.375	5.60	11.15	
$x_B, M_r, V/F$	1.392	6.05	11.37	
$x_B, M_r, B/L$	0.549	6.31	13.70	
x_B, M_r, L	837.4	6.68	22.95	
$x_B, M_r, V/L$	1.600	8.64	41.31	
$x_B, M_r, B/D$	0.916	11.2	47.77	
$x_B, M_r, F/F_0$	2.091	inf	inf	
$x_B, M_r, B/F$	0.478	inf	inf	
$x_B, M_r, D/F$	0.522	inf	inf	
x_B, M_r, D	502.0	inf	inf	
x_B, M_r, F	962.0	inf	inf	
$x_B, F/F_0, V/B$	—	inf	inf	
$x_B, F/F_0, x_D$	—	inf	inf	
$x_B, x_D, x_R(\text{BS})$	—	inf	inf	
$x_B, F/F_0, L/D$	—	inf	inf	
$x_B, F, x_D(\text{LS})$	—	inf	inf	
$V/B, F/F_0, x_D$	—	inf	inf	



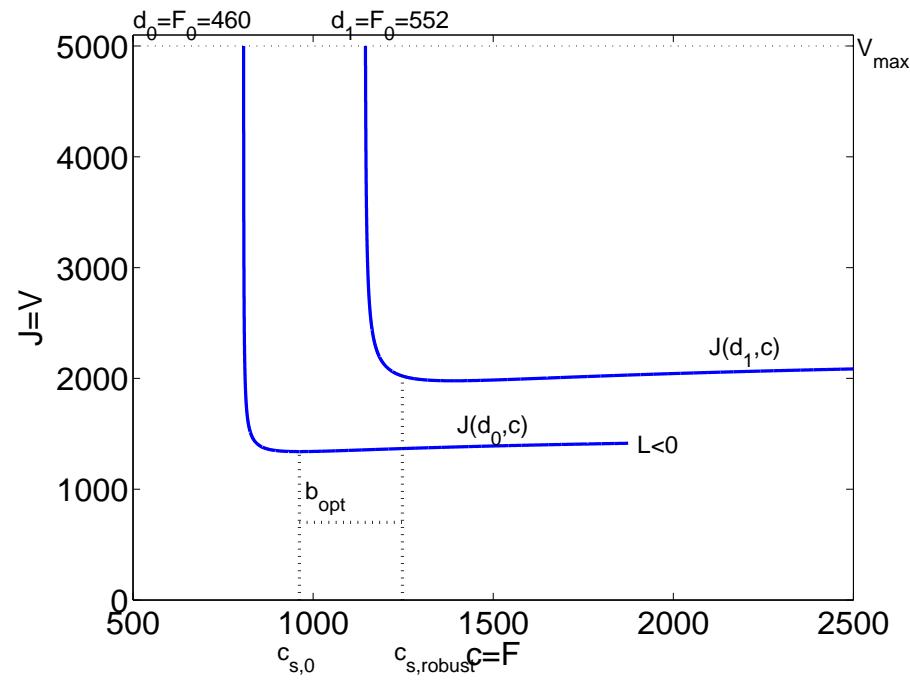
Conventional (x_D)



Larsson et.al. (L/F)



Finding optimal setpoints by robust optimization (Glemmestad et.al., 1998)



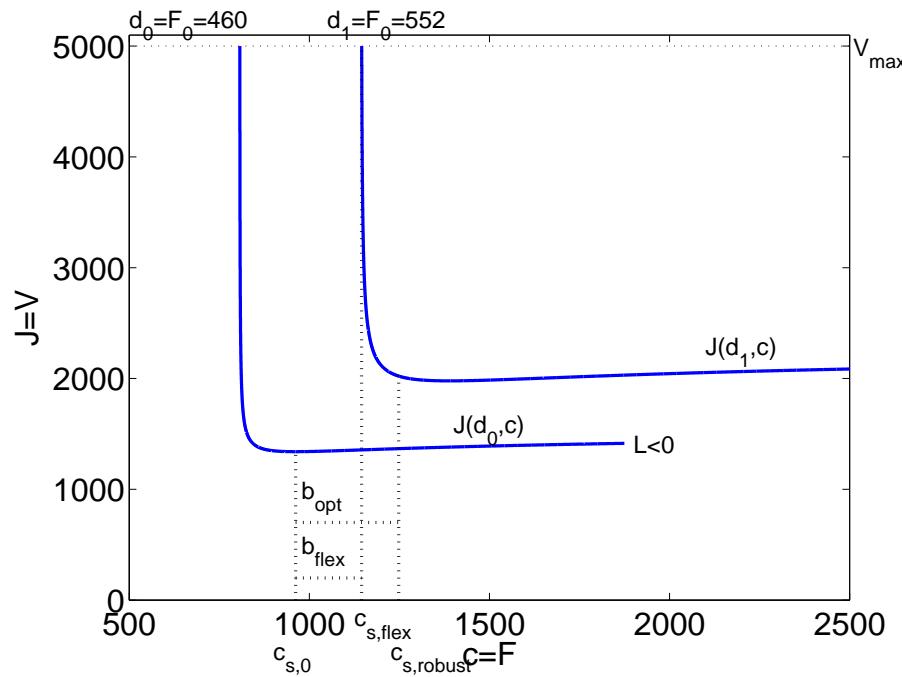
Robust optimization:

$$\begin{aligned} \min_{x_i, u_i, c_s} \sum_i w_i J(x_i, u_i, d_i) \\ f(x_i, u_i, d_i) = 0 \\ g(x_i, u_i, d_i) \leq 0 \\ c(x_i, u_i, d_i) = c_s + d_{c,i} \\ d_i = d_0 + \Delta d_i \\ d_{c,i} = d_{c,0} + \Delta d_{c,i} \\ \Delta d_i \in D_d, \quad \Delta d_{c,i} \in D_c \end{aligned}$$

“Optimal backoff”:

$$b_{opt} = c_{s,robust} - c_{s,0}$$

Finding flexible setpoints by online feasibility correction (Lid et.al., 2001)



Online feasibility correction:

$$\min_{x,u,c_{flex}} (c_{II,flex} - c_{II,s})^T Q_{II} (c_{II,flex} - c_{II,s})$$

$$f(x, u, d) = 0$$

$$g(x, u, d) + d_{g,max} - d_g \leq 0$$

$$c(x, u, d) = c_{flex} + d_c$$

$$c_{I,flex} = c_{I,s}$$

“Flexible backoff” :

$$b_{flex}(d, d_c) = c_{s,flex}(d, d_c) - c_{s,0}$$

Step 3: Loss evaluation

c_1, c_2, c_3	$c_{3,s}$	Nominal setpoints		$b_{3,opt}$	Robust setpoints		$b_{3,flex}^{max}$	Flexible setpoints	
		L_w (%)	L_{max} (%)		L_w (%)	L_{max} (%)		L_w (%)	L_{max} (%)
Reoptimized	$c_{opt}^*(d)$	5.16	11.03	–	5.16	11.03	–	4.97	11.03
x_B, M_r, x_D	0.825	5.22	11.04	0.005	5.21	11.03	0	5.22	11.04
$x_B, M_r, L/F$	0.871	5.39	11.24	-0.021	5.35	11.34	0	5.39	11.24
$x_B, M_r, D/L$	0.600	5.40	11.15	0.047	5.34	11.35	0	5.40	11.15
$x_B, M_r, D/V$	0.375	5.60	11.15	0.026	5.49	11.46	0	5.60	11.15
$x_B, M_r, V/F$	1.392	6.05	11.37	-0.037	5.93	11.67	0	6.05	11.37
$x_B, M_r, B/L$	0.549	6.31	13.70	0.054	6.05	12.60	0	6.31	13.70
x_B, M_r, L	837.4	6.68	22.95	-64	6.46	15.87	0	6.68	22.95
$x_B, M_r, V/L$	1.600	8.64	41.31	0.206	5.89	12.19	0	8.64	41.31
$x_B, M_r, B/D$	0.916	11.2	47.77	-0.140	6.00	11.68	0	11.2	47.77
$x_B, M_r, F/F_0$	2.091	inf	inf	0.289	6.22	12.15	0.1280	36.82	291.78
$x_B, M_r, B/F$	0.478	inf	inf	-0.056	6.36	12.08	0.0145	36.87	291.78
$x_B, M_r, D/F$	0.522	inf	inf	0.061	6.50	12.24	0.0242	36.89	291.78
x_B, M_r, D	502.0	inf	inf	191	6.79	12.82	91	26.63	165.24
x_B, M_r, F	962.0	inf	inf	286	7.51	13.90	183	26.90	165.24
$x_B, F/F_0, V/B$	–	inf	inf	–	25.87	54.38	0.6718	9.40	20.28
$x_B, F/F_0, x_D$	–	inf	inf	–	25.91	54.38	0.0001	8.24	24.36
$x_B, x_D, x_R(\text{BS})$	–	inf	inf	–	26.08	54.38	0	6.36	16.24
$x_B, F/F_0, L/D$	–	inf	inf	–	33.13	63.59	0.0001	10.06	26.59
$x_B, F, x_D(\text{LS})$	–	inf	inf	–	43.10	94.37	0.1735	30.84	165.24
$V/B, F/F_0, x_D$	–	inf	inf	–	45.74	78.75	0.0321	8.95	28.28

Step 4: Final evaluation and selection of control structure

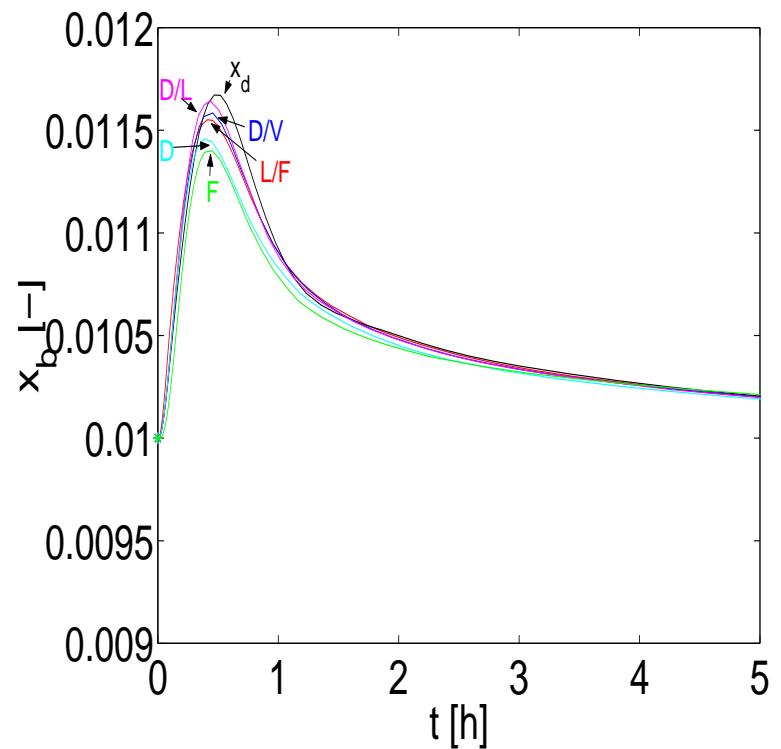
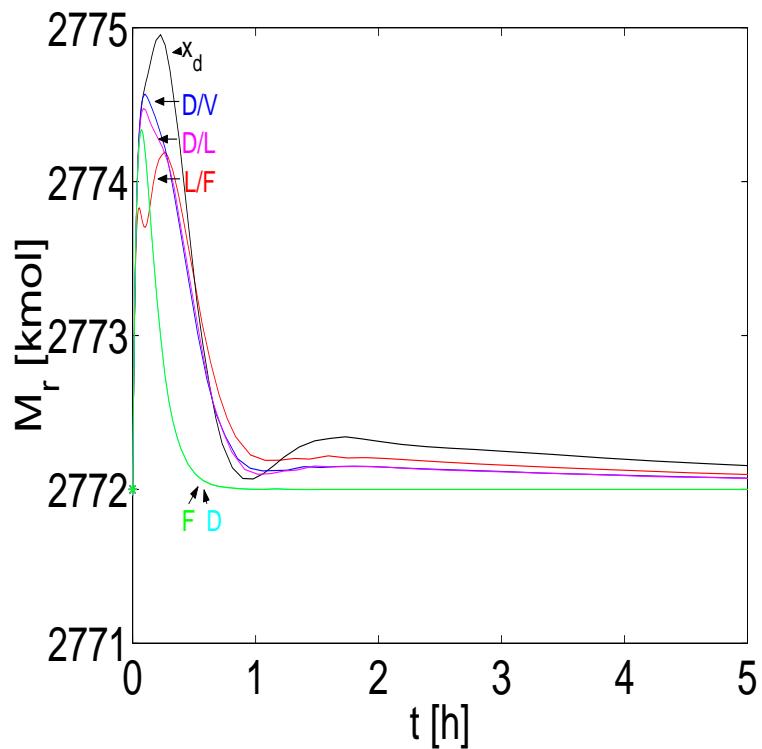
Stabilize reboiler, condenser and reactor holdup

Pairing based on relative gain array (RGA):

Alt.	Loop 1	Loop 2	Loop 3	Loop 4	Loop 5
x_d	$M_b \leftrightarrow B$	$M_d \leftrightarrow D$	$M_r \leftrightarrow F$	$x_b \leftrightarrow V$	$x_d \leftrightarrow L$
L/F	$M_b \leftrightarrow B$	$M_d \leftrightarrow D$	$M_r \leftrightarrow F$	$x_b \leftrightarrow V$	$L/F \leftrightarrow L$
D/L	$M_b \leftrightarrow B$	$M_d \leftrightarrow D$	$M_r \leftrightarrow F$	$x_b \leftrightarrow V$	$D/L \leftrightarrow L$
D/V	$M_b \leftrightarrow B$	$M_d \leftrightarrow D$	$M_r \leftrightarrow F$	$x_b \leftrightarrow V$	$D/V \leftrightarrow L$
F	$M_b \leftrightarrow B$	$M_d \leftrightarrow L$	$M_r \leftrightarrow D$	$x_b \leftrightarrow V$	F
D	$M_b \leftrightarrow B$	$M_d \leftrightarrow L$	$M_r \leftrightarrow F$	$x_b \leftrightarrow V$	D

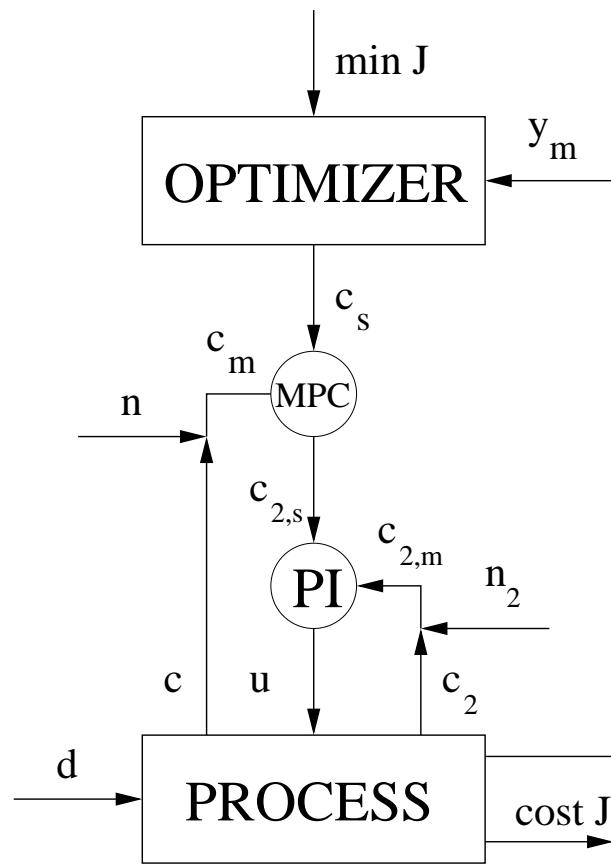
All six alternatives show good controllability.

Robust optimal setpoints
Disturbance: $\Delta F_0 = +20\%$



Control: All alternatives OK

Plantwide control (Chap. 5-6)



Important tasks:

- Controlled variables
- Manipulated variables
- Measurements
- Control configuration
- Controller type

Plantwide control procedure
(Larsson et.al., 2001):

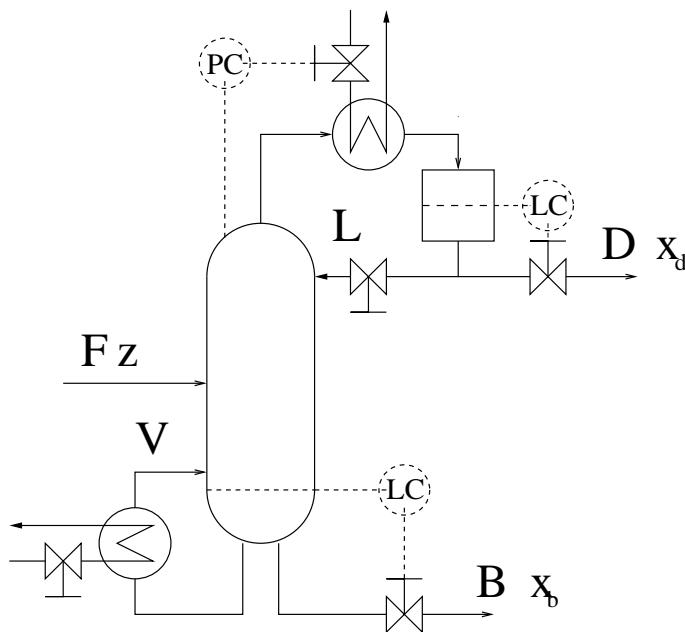
- Top-down analysis
- Bottom-up design

Case-studies:

- Combined-cycle power plant
- Heat-integrated distillation column

Two-point composition control in distillation: Optimal number of stages wrt. controllability

Fixed setpoints:



- Two competing factors:
 - Interaction:
Smallest with many stages
Reference tracking
 - Internal flows:
Largest with few stages
Disturbance rejection

Fixed energy
(constant internal flows):

- Best with many stages

Further work

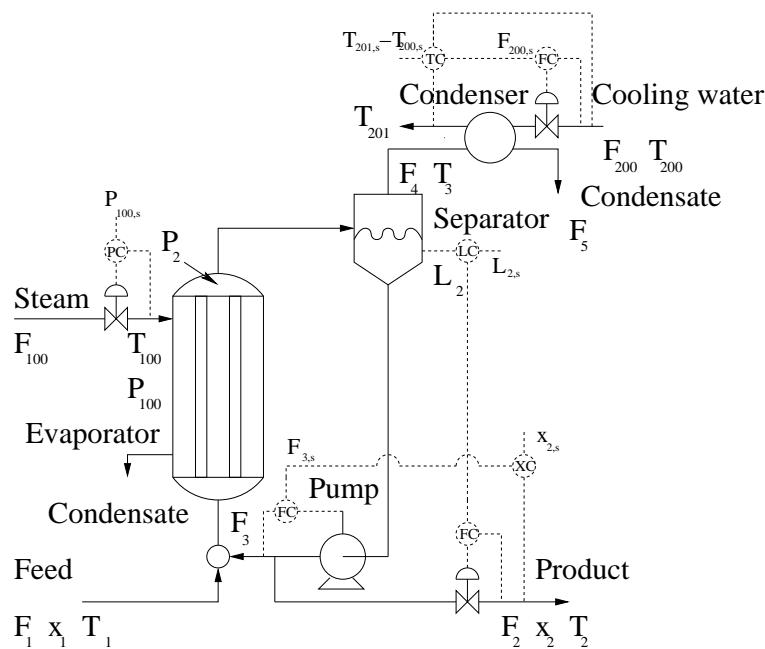
- Identifying candidate controlled variables
- Model uncertainty
- Plantwide control procedure: Bottleneck, degree of freedom, bottom-up design.
- Case-studies

Concluding remarks

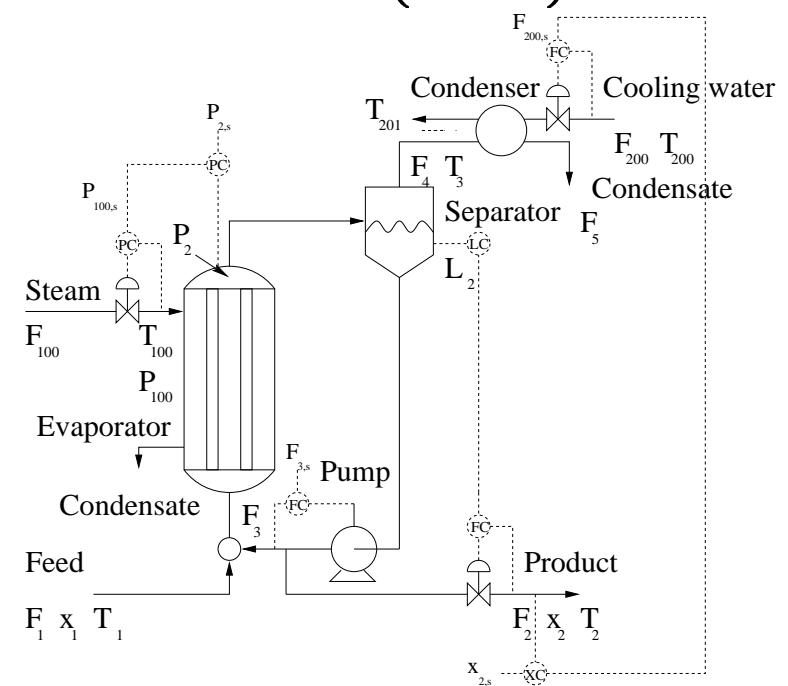
- Self-optimizing control and feasibility
- Several detailed case-studies based on a systematic method.

Example 3: Evaporation process (Newell, 1989)

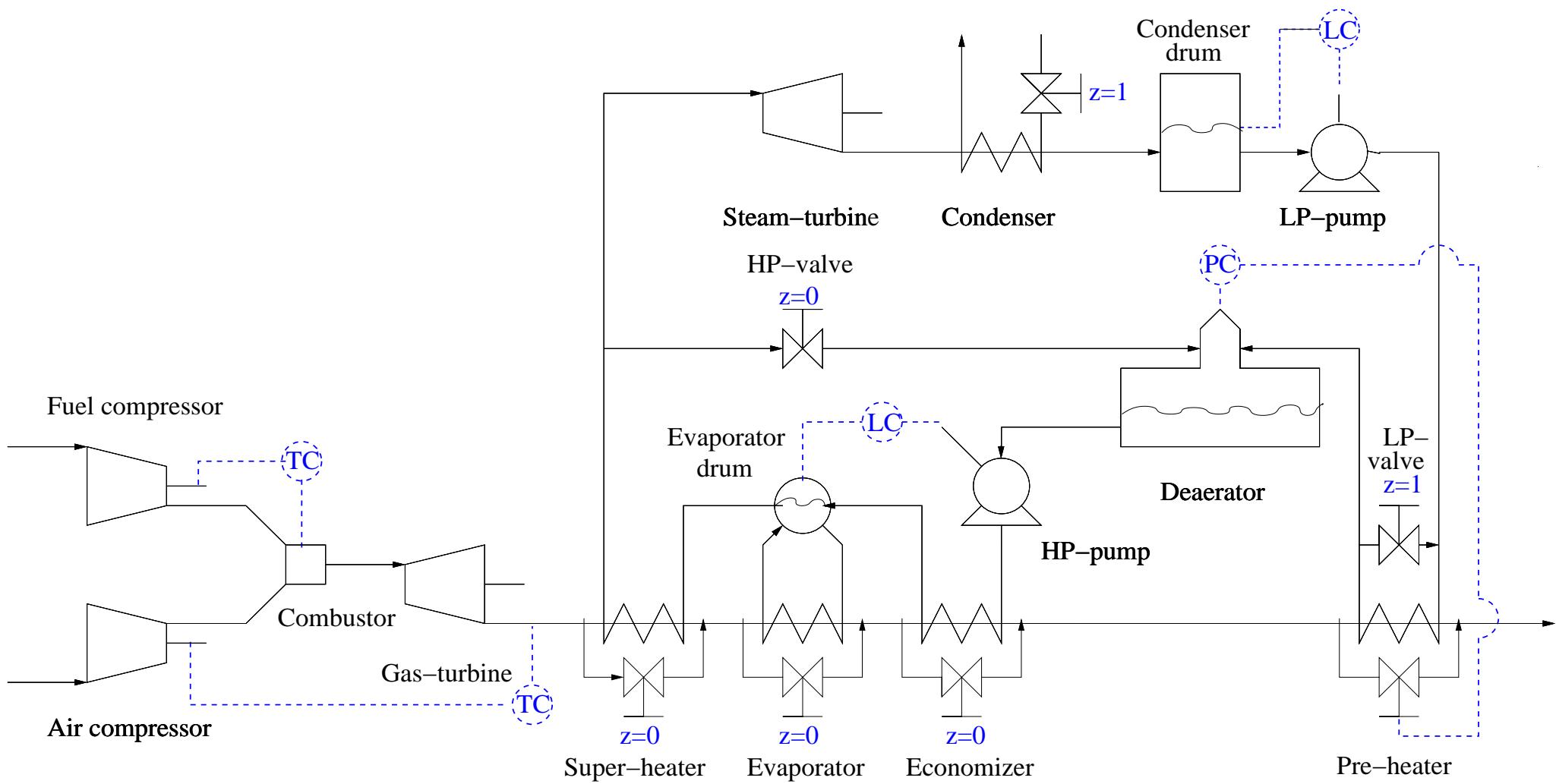
$T_{201} - T_{200}$



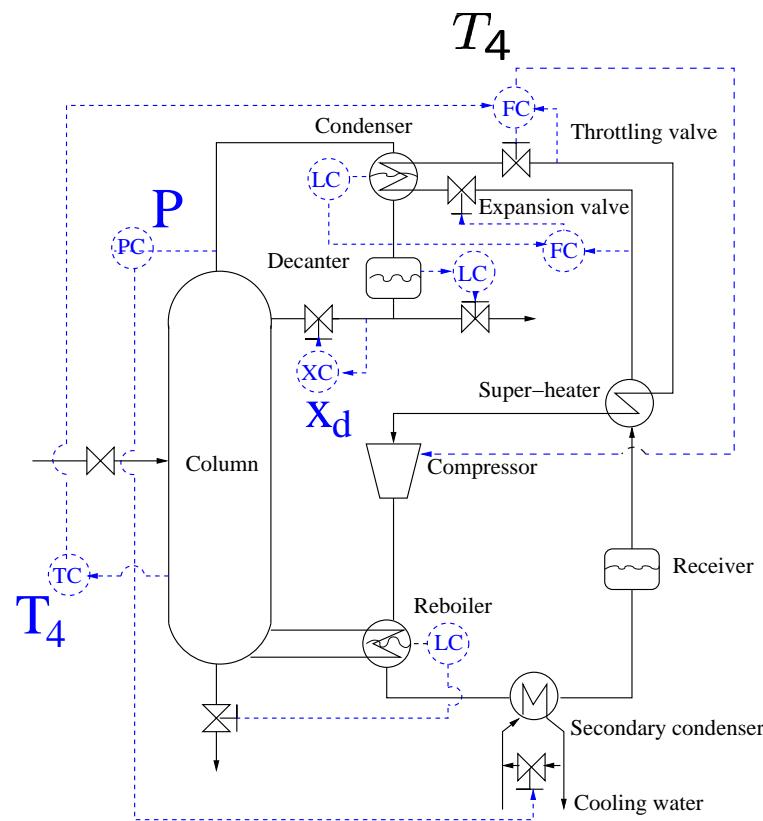
Kookos et.al.(2001)



Case study 1: Combined cycle power plant



Case study 2: Heat-integrated distillation column



Li et.al.(2003)

