# Self-Optimizing Control and NCO tracking

in the Context of Real-Time Optimization

DYCOPS 2010, Leuven

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Norwegian University of Science and Technology (NTNU)

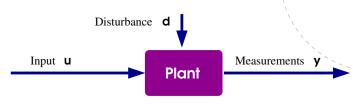
Trondheim



# **Outline**

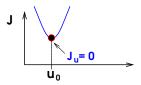
- 1. Introduction
- 2. NCO-tracking
- 3. Self-optimizing control (SOC)
- 4. Properties of NCO tracking and SOC
- 5. Combine methods
- 6. CSTR Example
- 7. Conclusions

### 1. Introduction

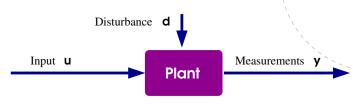


- Steady state optimization of continuous processes
- · Objective:

$$\min_{\boldsymbol{u}} \boldsymbol{\mathit{J}}(\boldsymbol{u},\boldsymbol{d}) \quad \text{s.t.} \quad \boldsymbol{\mathit{S}}(\boldsymbol{u},\boldsymbol{d}) \leq 0.$$

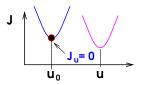


### 1. Introduction



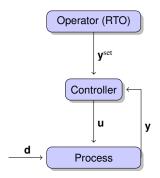
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## Introduction – Conclusion preview

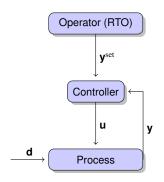
In practice



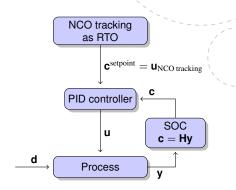
We propose.

## Introduction - Conclusion preview

## In practice



## We propose.



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• Origin: Batch-to-Batch optimization

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(Srinivasan 2002, François 2005, Srinivasan 2008)

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Idea: Track the optimality conditions using measurements

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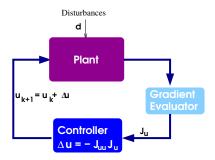
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- Idea: Track the optimality conditions using measurements
  - Measurements: Measured and estimated quantities

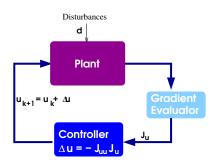
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· Unconstrained optimization

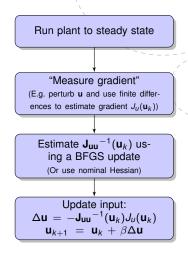


- Iteratively update u
- Push sensitivities  $J_{ii}$  to zero.

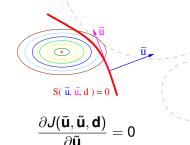
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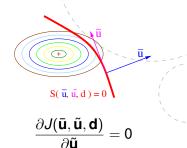


$$\mathcal{S}(\bar{\boldsymbol{u}},\tilde{\boldsymbol{u}},\boldsymbol{d})=0$$

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$$\Delta \bar{\boldsymbol{u}} = -\left(\frac{\partial \boldsymbol{\mathcal{S}}(\bar{\boldsymbol{u}}, \tilde{\boldsymbol{u}}, \boldsymbol{d})}{\partial \bar{\boldsymbol{u}}}\right)^{-1} \boldsymbol{S_{\!m}}$$

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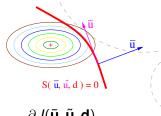
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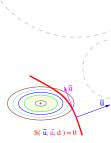
$$\mathcal{S}(\bar{\boldsymbol{u}},\tilde{\boldsymbol{u}},\boldsymbol{d})=0$$

$$\mathbf{u}^{\textit{new}} = \mathbf{u}^{\textit{old}} + \beta \Delta \mathbf{u}$$

Step length parameter:  $\beta$ 

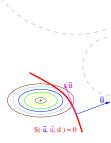
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- Gradient is generally difficult to measure
  - Finite difference
  - Model

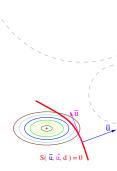


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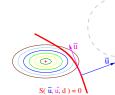
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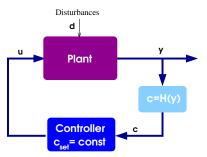
#### Weaknesses

- Existing knowledge about disturbances is not used
- Online (intermediate/transient) measurements not used
- Discrete input updates
  - Active constraints satisfied iteratively (⇔ Feedback)



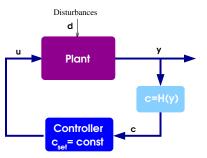
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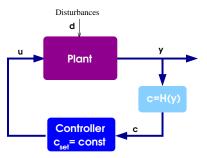
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• SOC addresses the question: How to select H?

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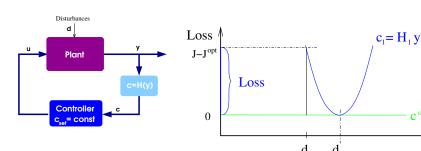
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Definition (Skogestad (2000))

Self-optimizing control is when we can achieve an acceptable loss with constant setpoint values for the controlled variables

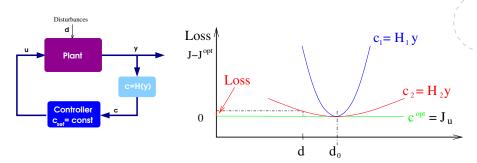
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Interpretation: Find good and simple approximation to  $J_u$  using online measurements  $\mathbf{v}$ 

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- Single measurements:

$$\mathbf{c} = \mathbf{H}\mathbf{y} \qquad \mathbf{H} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \end{bmatrix}$$

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Combinations of measurements:

$$\mathbf{c} = \mathbf{H}\mathbf{y}$$
  $\mathbf{H} = \begin{bmatrix} h_{11} & h_{12} & h_{13} & h_{14} \\ h_{21} & h_{22} & h_{23} & h_{24} \end{bmatrix}$ 

e.g. ratio control

Null space method

$$\min_{u} \textit{J}(u,d) = [u\,d] \left[ \begin{array}{cc} J_{uu} & J_{ud} \\ J_{ud}^{T} & J_{dd} \end{array} \right] \left[ \begin{array}{c} u \\ d \end{array} \right]$$

- Linear measurement model  $\mathbf{y} = \mathbf{G}^{y}\mathbf{u} + \mathbf{G}_{d}^{y}\mathbf{d}$
- Linear Measurement combinations  $\mathbf{c} = \mathbf{H} \mathbf{y}$

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#### **Theorem**

Given a sufficient number of measurements ( $n_y \ge n_u + n_d$ ) and no measurement noise, select **H** such that

$$HF = 0$$

where

$$\mathbf{F} = \frac{\partial \mathbf{y}^{opt}}{\partial \mathbf{d}}$$

-Controlling  $\mathbf{c} = \mathbf{H}\mathbf{y}$  to zero yields locally zero loss from optimal operation.

Proof

$$\begin{split} \textbf{F} &= \frac{\partial \textbf{y}^{opt}}{\partial \textbf{d}} \\ \textbf{y}^{opt}(\textbf{d}) &- \textbf{y}^{opt}(\textbf{d}_0) = \textbf{F}(\textbf{d} - \textbf{d}_0) \end{split}$$

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#### Obtaining F

- · Assume set of disturbances d
- Numerically find  $\mathbf{F} = \frac{\Delta \mathbf{y}^{opt}}{\Delta \mathbf{d}}$
- From  $\mathbf{F} = -\mathbf{G}^y \mathbf{J_{uu}}^{-1} \mathbf{J_{ud}} + \mathbf{G}_d^y$  where  $\mathbf{J_{uu}} = \frac{\partial^2 J}{\partial \mathbf{u}^2}$  and  $\mathbf{J_{ud}} = \frac{\partial J}{\partial \mathbf{d}}$

## 4. Properties of NCO tracking and SOC

## Self-optimizing control

 $\bullet \ \ \text{Procedure for finding } \textbf{c} = \textbf{Hy} \\$ 

## NCO tracking

• Controlled variable: Ju

### Self-optimizing control

- Procedure for finding **c** = **Hy**
- Ju and Jacobian not measured

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  - ⇒ Lower control layer

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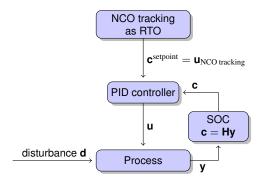
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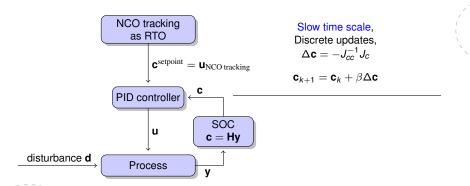
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⇒ RTO layer

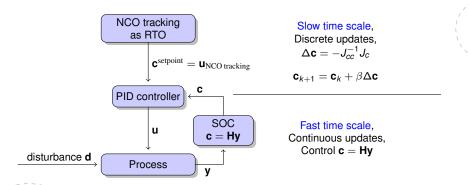
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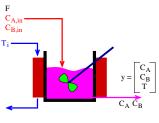
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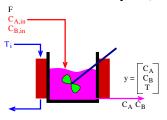
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- Smooth inputs u
- Expected disturbances rejected fast by SOC (lower layer)
- Unexpected disturbances rejected on a slow time scale by NCO tracking (RTO layer)
- Gradient measurements not required so frequently.



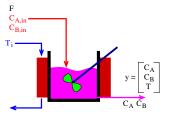
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#### Disturbance (d):

Feed Concentration  $C_{A,in}$ Feed Concentration  $C_{B,in}$ 



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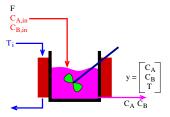
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 $C_{A,in}$  $C_{B,in}$ 

Input (u):

Jacket temperature

 $T_i$ 



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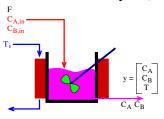
Input (u):

Jacket temperature  $T_i$ 

Measurements (y):

Concentration  $C_A$ 

Concentration  $C_B$ Temperature T



$$A \Rightarrow B$$

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Feed Concentration  $C_{A,in}$ Feed Concentration  $C_{B,in}$ 

Input (u):

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Measurements (y):

 $\begin{array}{ccc} \text{Concentration} & & & C_A \\ \text{Concentration} & & & C_B \\ \text{Temperature} & & & T \\ \end{array}$ 

$$\frac{dC_A}{dt} = \frac{1}{\tau} (C_{A,in} - C_A) - r$$

$$\frac{dC_B}{dt} = \frac{1}{\tau} (C_{B,in} - C_B) + r$$

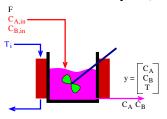
$$\frac{dT}{dt} = \frac{1}{\tau} (T_i - T) + \frac{-\Delta H_{rx}}{\rho C_p} r$$

$$r = k_1 C_A - k_2 C_B$$
$$k_1 = K_1 e^{\frac{-E_1}{RT}}$$
$$k_2 = K_2 e^{\frac{-E_2}{RT}}$$

 $T_i$ 

 $C_A$ 

 $C_B$ 



$$A \rightleftharpoons B$$

#### Disturbance (d):

Feed Concentration  $C_{A,in}$ Feed Concentration  $C_{B,in}$ 

Input (u):

Jacket temperature

#### Measurements (v):

Concentration Concentration Temperature

$$\frac{dC_B}{dt} = \frac{1}{\tau} (C_{B,in} - C_B) + r$$

$$\frac{dT}{dt} = \frac{1}{\tau} (T_i - T) + \frac{-\Delta H_{rx}}{\rho C_p} r$$

$$r = k_1 C_A - k_2 C_B$$

 $\frac{dC_A}{dt} = \frac{1}{\tau}(C_{A,in} - C_A) - r$ 

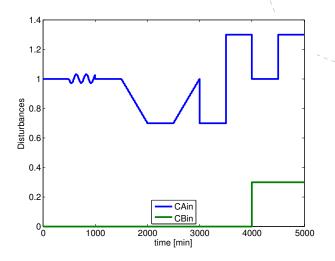
$$k_1 = K_1 e^{\frac{-E_1}{RT}}$$
  
 $k_2 = K_2 e^{\frac{-E_2}{RT}}$ 

Objective: Maximize Profit

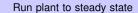
$$\max_{T_i} J = p_{C_B} C_B - (p_{T_i} T_i)^2$$

Noise: offset -0.1, std dev: 0.2

# CSTR Example - Disturbances (d)







Perturb  $\mathbf{u}$  and run plant to steady state to estimate  $J_u(\mathbf{u}_k)$ 

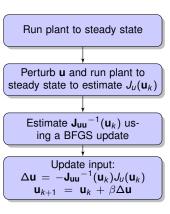
Estimate  $\mathbf{J_{uu}}^{-1}(\mathbf{u}_k)$  using a BFGS update

Update input:  

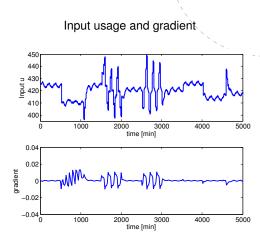
$$\Delta \mathbf{u} = -\mathbf{J}_{\mathbf{u}\mathbf{u}}^{-1}(\mathbf{u}_k)J_{u}(\mathbf{u}_k)$$
  
 $\mathbf{u}_{k+1} = \mathbf{u}_k + \beta\Delta\mathbf{u}$ 

Sampling time  $T_S = 10 \text{ min}$ Perturbation  $\Delta T_{pert} = 1 \text{ K}$ Step size  $\beta = 0.4$ 



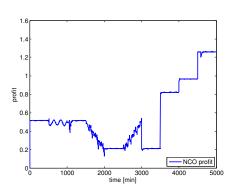


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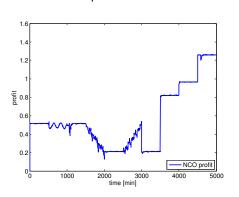
#### Instantaneous profit



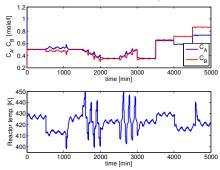
#### Concentrations and reactor temperature



#### Instantaneous profit



#### Concentrations and reactor temperature





#### Self-optimizing control

- Cost is not measured
- Select **H** such that **HF** = 0

$$\mathbf{F} = \frac{\partial \mathbf{y}^{op}}{\partial \mathbf{d}}$$

c = Hy

#### Controlled variable:

$$-0.769$$
 $C_A + 0.639$  $C_B + 0.005$  $T$ 



### Self-optimizing control

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- Select **H** such that **HF** = 0

$$\mathbf{F} = \frac{\partial \mathbf{y}^{opt}}{\partial \mathbf{d}}$$

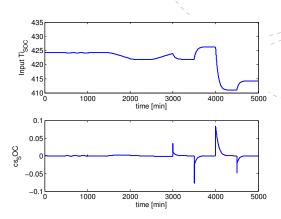
• c = Hy

#### Controlled variable:

$$\mathbf{c} =$$

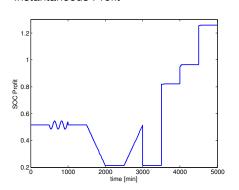
$$-0.769$$
 $C_A + 0.639$  $C_B + 0.005$  $T$ 

Input and controlled variable c





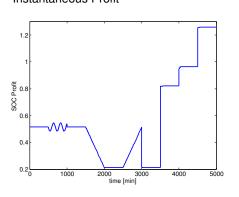
#### Instantaneous Profit



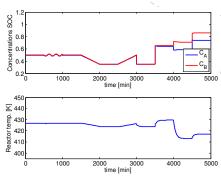
#### Concentrations and reactor temperature



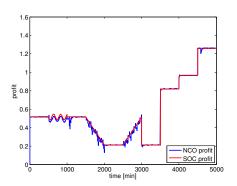
#### Instantaneous Profit



#### Concentrations and reactor temperature



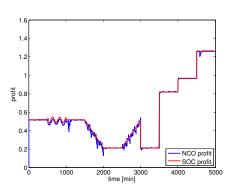
Comparing instantaneous profit



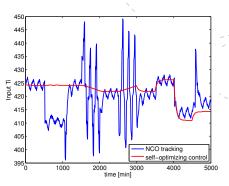




#### Comparing instantaneous profit

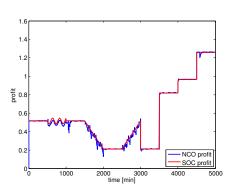


### Comparing input usage

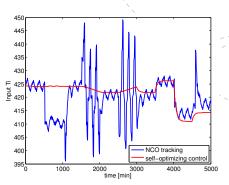




Comparing instantaneous profit



Comparing input usage



Winner so far: SOC

# CSTR Example – Unexpected disturbance in $E_2$

• New disturbance: Activation Energy E<sub>2</sub> changes +10%

$$\textit{k}_2 = \textit{K}_2 e^{\frac{-\textit{E}_2}{\textit{RT}}}$$

Reaction rate:

$$r = k_1 C_A - k_2 C_B$$

Favours formation of product B

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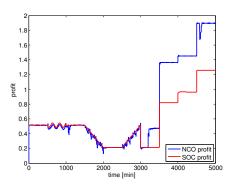
Reaction rate:

$$r = k_1 C_A - k_2 C_B$$

- Favours formation of product B
- Not taken into account when calculating  $\mathbf{F} = \frac{\partial \mathbf{y}^{opt}}{\partial \mathbf{d}}$

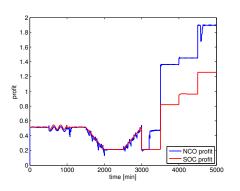
# CSTR Example – Unexpected disturbance in $E_2$

Instantaneous profit



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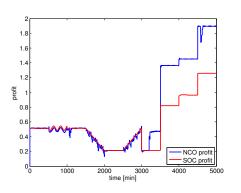
Instantaneous profit

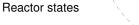


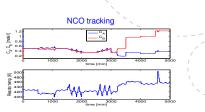
Reactor states

## CSTR Example – Unexpected disturbance in $E_2$

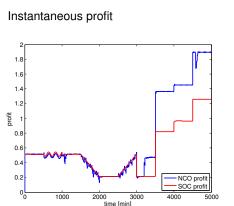
Instantaneous profit

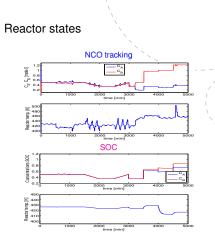




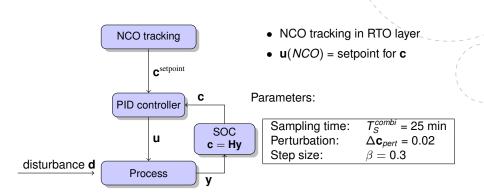


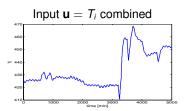
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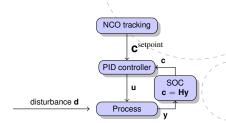


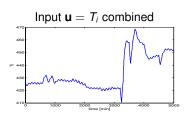


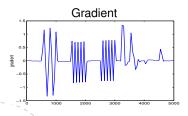
Winner this time: NCO tracking

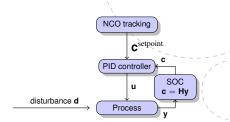


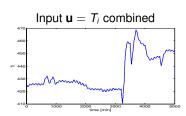


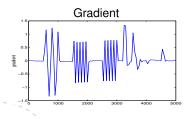


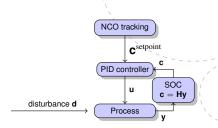


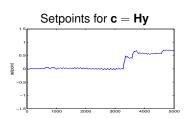




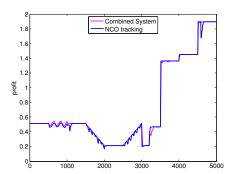


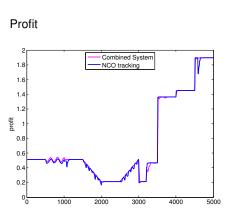


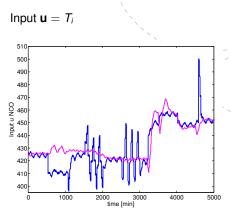




#### Profit







NCO tracking and SOC

• Have the same purpose:

NCO tracking and SOC

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 $\min J(\mathbf{u}, \mathbf{d})$ 

Are not competing methods

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  - less perturbations and discrete input changes
- Use SOC in the lower layer

## Thank you

