

CONTROL STRUCTURE DESIGN

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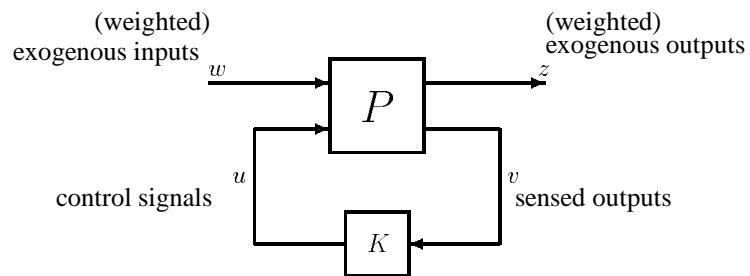
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This is a copy of the transparencies used for the presentation. For more detailed information see Chapter 10 in S. Skogestad and I. Postlethwaite, *Multivariable feedback control - Analysis and design*, Wiley, 1996.

THEORY: General formulation



- Find a controller K which based on the information in v , generates a control signal u which counteracts the influence of w on z , thereby minimizing the closed-loop norm from w to z .

PRACTICE: Typical base level control structure

PRACTICE: Typical control hierarchy

Foss (1973):

The central issue to be resolved ... is the determination of control system structure.

Which variables should be measured, which inputs should be manipulated and which links should be made between the two sets?

There is more than a suspicion that the work of a genius is needed here, for without it the control configuration problem will likely remain in a primitive, hazily stated and wholly unmanageable form.

The gap is present indeed, but contrary to the views of many, it is the theoretician who must close it.

CONTROL STRUCTURE DESIGN

Tasks:

1. *Selection of controlled outputs* (a set of variables which are to be controlled to achieve a set of specific objectives)
2. *Selection of manipulations and measurements* (sets of variables which can be manipulated and measured for control purposes)
3. *Selection of **control configuration*** (a structure interconnecting measurements/commands and manipulated variables)
4. *Selection of controller type* (control law specification, e.g., PID, decoupler, LQG, etc.).

Note distinction between control *structure* and control *configuration*.

Tasks 1 and 2 combined: *input/output selection*

Task 3 (configuration): *input/output pairing*

Shinskey (1967, 1988)

Morari (1982)

Stephanopoulos (1984)

Balchen and Mumme (1988)

Nett (1989)

van de Wal and de Jager (1995)

Skogestad and Postlethwaite (1996)

TASK 1: Selection of controlled outputs

Controlled output y : Measured output with reference (r)

Two distinct questions:

1. What should the controlled variables y ?
(includes open-loop by selecting $y = u$)
2. What is their optimal values (y_{opt})?

Second problem: Extensively studied.

Example 1. Room heating.

y = room temperature

Other cases: Less obvious.

Example 2. Cake baking.

Goal (purpose): well baked inside and nice outside

Manipulated input: $u = Q$ (assume 15 minutes).

(a) Open-loop implementation: Heat input Q

(b) Closed-loop implementation:

y = oven temperature

“Optimizer”: Cook book (look-up table)

SELECTION OF CONTROLLED OUTPUTS

The input u (generated by feedback to achieve $y \approx r$) should be close to the optimal input $u_{\text{opt}}(d)$.

$$u - u_{\text{opt}} = G^{-1}(0)(y - y_{\text{opt}})$$

where

$$y - y_{\text{opt}} = \underbrace{y - r}_e + \underbrace{r - y_{\text{opt}}(d)}_{e_{\text{opt}}}$$

\Rightarrow Select controlled outputs y such that:

1. $G^{-1}(0)$ is small; inputs have a large effect on y .
2. $e_{\text{opt}} = r - y_{\text{opt}}(d)$ is small; $y_{\text{opt}}(d)$ depends only weakly on disturbances.
3. $e = y - r$ is small; good measurement and control of y .

Scale outputs such that $\|y - y_{\text{opt}}(d)\| \approx 1$ (due to measurement errors and disturbances)

Note: $\bar{\sigma}(G^{-1}(0)) = 1/\underline{\sigma}(G(0))$.

Conclusion. Simple tool:

- Prefer a set of controlled outputs with large $\underline{\sigma}(G(0))$.

Distillation column example from Kjetil

Distillation column example from Kjetil

Distillation column example from Kjetil

TASK 2: Selection of manipulations and measurements

- y – all candidate outputs (measurements)
- u – all candidate inputs (manipulations)

Combinatorial growth: Detailed analysis time consuming.

Possibilities with 1 to M inputs and 1 to L outputs (Nett, 1989):

$$\sum_{m=1}^M \sum_{l=1}^L \binom{L}{l} \binom{M}{m}$$

$M = L = 2$: $4+2+2+1=9$ candidates

$M = L = 4$: 225 candidates, etc.

TOOLS THAT AVOID COMBINATORIAL GROWTH DESIRED.

RGA is one such tool.

RGA for non-square plant

$$\Lambda(G) = G \times G^\dagger$$

HDA plant (Cao, 1995).

- 5 outputs and 13 candidate inputs.
- $\binom{13}{5} = 1287$ combinations with 5 inputs / 5 outputs.
- $\binom{13}{6} = 1716$ combinations with 6 inputs / 5 outputs.

$$G^T(0) = \begin{bmatrix} 0.7878 & 1.1489 & 2.6640 & -3.0928 & -0.0703 \\ 0.6055 & 0.8814 & -0.1079 & -2.3769 & -0.0540 \\ 1.4722 & -5.0025 & -1.3279 & 8.8609 & 0.1824 \\ -1.5477 & -0.1083 & -0.0872 & 0.7539 & -0.0551 \\ 2.5653 & 6.9433 & 2.2032 & -1.5170 & 8.7714 \\ 1.4459 & 7.6959 & -0.9927 & -8.1797 & -0.2565 \\ 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 \\ 0.1097 & -0.7272 & -0.1991 & 1.2574 & 0.0217 \\ 0.3485 & -2.9909 & -0.8223 & 5.2178 & 0.0853 \\ -1.5899 & -0.9647 & -0.3648 & 1.1514 & -8.5365 \\ 0.0000 & 0.0002 & -0.5397 & -0.0001 & 0.0000 \\ -0.0323 & -0.1351 & 0.0164 & 0.1451 & 0.0041 \\ -0.0443 & -0.1859 & 0.0212 & 0.1951 & 0.0054 \end{bmatrix}$$

RGA may be useful in providing an initial screening:

$$\Lambda^T = \begin{bmatrix} 0.1275 & -0.0755 & 0.5907 & 0.1215 & 0.0034 \\ 0.0656 & -0.0523 & 0.0030 & 0.1294 & 0.0002 \\ 0.2780 & 0.0044 & 0.0463 & 0.4055 & -0.0060 \\ 0.3684 & -0.0081 & 0.0009 & 0.0383 & -0.0018 \\ -0.0599 & 0.9017 & 0.2079 & -0.1459 & 0.0443 \\ 0.1683 & 0.4042 & 0.1359 & 0.1376 & 0.0089 \\ 0.0000 & 0.0000 & 0.0000 & 0.0000 & 0.0000 \\ 0.0014 & -0.0017 & 0.0013 & 0.0099 & 0.0000 \\ 0.0129 & -0.0451 & 0.0230 & 0.1873 & -0.0005 \\ 0.0374 & -0.1277 & -0.0359 & 0.1163 & 0.9516 \\ 0.0000 & 0.0000 & 0.0268 & 0.0000 & 0.0000 \\ 0.0001 & 0.0001 & 0.0000 & 0.0001 & 0.0000 \\ 0.0002 & 0.0002 & 0.0001 & 0.0001 & 0.0000 \end{bmatrix}, \quad \Lambda_{\Sigma}^T = \begin{bmatrix} 0.77 \\ 0.15 \\ 0.73 \\ 0.40 \\ 0.95 \\ 0.85 \\ 0.00 \\ 0.01 \\ 0.18 \\ 0.94 \\ 0.03 \\ 0.00 \\ 0.00 \end{bmatrix}$$

- Five inputs with the largest inputs projection: 5, 10, 6, 1, and 3 (in that order).
- For this selection $\underline{\sigma}(G_s) = 1.73$ whereas $\underline{\sigma}(G) = 2.45$ for the overall system.

TASK 3: Selection of control configuration

Controller K connects available measurements/commands (v) and manipulations (u):

$$u = Kv$$

Control configuration: *The restrictions imposed on the structure of the overall controller K by decomposing it into a set of local controllers (subcontrollers, units, elements, blocks) with predetermined links and with a possibly predetermined design sequence.*

Typical restriction: one degree-of-freedom controller where input is $r - y$.

Some elements used to build up configuration:

- Decentralized controllers (K diagonal)
- Cascade controllers (predetermined order for tuning)
- Feedforward elements
- Decoupling elements
- Selectors

Decentralized control. *The control system consists of independent feedback controllers which interconnect a subset of the output measurements/commands and a subset of the manipulated inputs. These subsets should not be used by any other controller.*

Usually: Rearrange order of inputs and outputs such that K is block-diagonal.

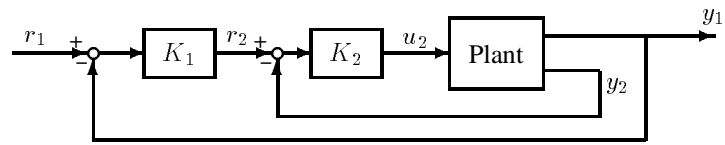
Cascade control *is when the output from one controller is the input to another. This is broader than the conventional definition of cascade control which is that the output from one controller is the reference command (setpoint) to another.*

Feedforward elements *link measured disturbances and manipulated inputs.*

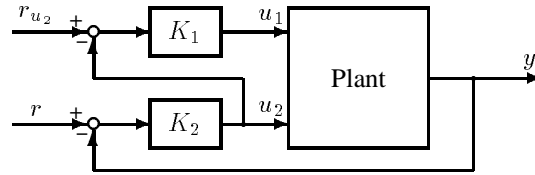
Decoupling elements *link one set of manipulated inputs (“measurements”) with another set of manipulated inputs. Often viewed as “feedforward” elements.*

In addition to restriction on structure on K : Impose restrictions on *sequence* the subcontrollers are designed.

Cascaded controllers



(a) Extra measurements y_2 (conventional cascade control)



(b) Extra inputs u_2 (input resetting)

Why use control configurations?

- Decomposed configurations often quite complex.
- Better performance: Optimization problem – resulting in a centralized multivariable controller.

So why use control configurations?

- Cost associated with obtaining good plant models (needed for centralized control).
- Cascade, decentralized, etc.: Controller is usually tuned one at a time with little modelling effort. Often ON-LINE tuning.

Other advantages decentralized/cascade/hierarchical configurations:

- Often easier to understand for operators
- Reduce the need for control links
- Allow for decentralized implementation
- Tuning parameters have direct and “localized” effect
- Tend to be insensitive to uncertainty
- Simpler implementation
- Reduced computation load
- Simple or even on-line tuning
- Longer sampling intervals for the higher layers
- Allow simple models when designing higher layers
- “Stabilize”¹ the plant such that it is can be controlled by operators.

¹The terms “stabilize” and “unstable” as used by process operators may not refer to a plant that is unstable in a mathematical sense, but rather to a plant that is *sensitive* to disturbances and which is difficult to control manually.

THEORY FOR CONTROL CONFIGURATIONS

Partial control

	Meas./Control of y_1 ?	Control objective for y_2 ?
Sequential decentralized control	Yes	Yes
Sequential cascade control	Yes	No
“True” partial control	No	Yes
Indirect control	No	No

Set $y_2 = r_2$

$$y_1 = \underbrace{(G_{11} - G_{12}G_{22}^{-1}G_{21})}_{\triangleq P_u} u_1 + \underbrace{(G_{d1} - G_{12}G_{22}^{-1}G_{d2})}_{\triangleq P_d} d + \underbrace{G_{12}G_{22}^{-1}}_{\triangleq P_r} (r_2 - n_2)$$

P_d – partial disturbance gain

Some criteria for selecting u_2 and y_2 in lower-layer:

1. Lower layer must quickly implement the set-points from higher layers, i.e., controllability of subsystem u_2/ y_2 should be good. (G_{22})
2. Provide for local disturbance rejection. (P_d)
3. Impose no unnecessary control limitations on problem involving u_1 and/or r_2 to control y_1 . (P_u or P_r)

“Unnecessary”: Limitations (RHP-zeros, ill-conditioning, etc.) not in original problem involving u and y

Example: Control of 5×5 distillation process

$$u = [L \quad V \quad D \quad B \quad V_T]^T$$

$$y = [y_D x_B \quad M_D \quad M_B \quad p]^T$$

Stabilize: Close three SISO loops for level and pressure:

$$y_1 = [y_D \quad x_B]^T, \quad y_2 = [M_D \quad M_B \quad p]^T$$

Many possible choices for u_1 and u_2 . *LV*-configuration:

$$u_1 = [L \quad V]^T$$

DV-configuration:

$$u_1 = [D \quad V]^T$$

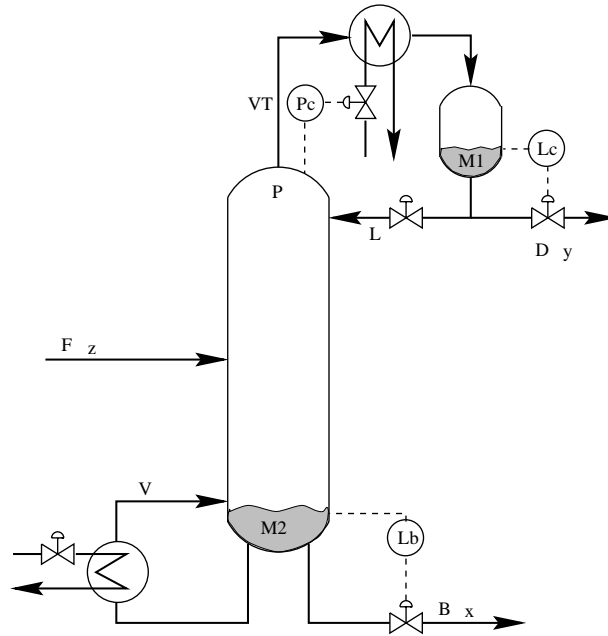


Figure 6: Typical distillation column with LV-control configuration

- 5×5 model.

Important issues:

- Disturbance sensitivity (P_d should be small)
- Interactions (RGA-elements of P_u)

Because of interactions and cost of measurements:
Often only one product composition controlled (“true” partial control).

Decentralized feedback control

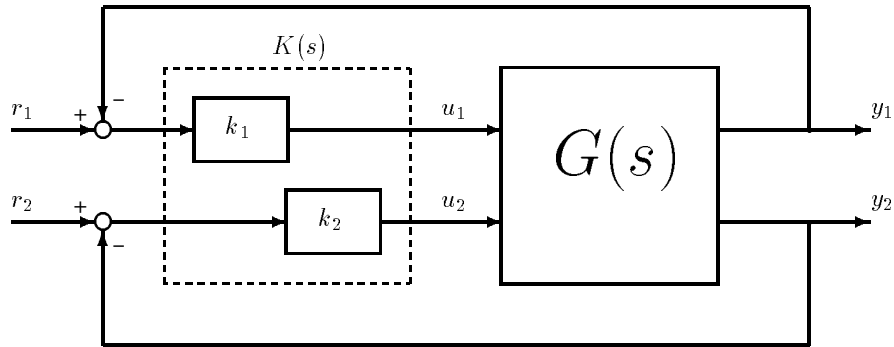


Figure 8: Decentralized diagonal control of a 2×2 plant

Design of decentralized control systems involves two steps:

1. Choice of pairings (control configuration selection)
2. Design (tuning) of each controller, $k_i(s)$.

Magnitude of off-diagonal elements in G relative to its diagonal elements given by:

$$E \triangleq (G - \tilde{G}_{diag})\tilde{G}_{diag}^{-1}$$

Important relationship:

$$\underbrace{(I + GK)}_{\text{overall}} = \underbrace{(I + E\tilde{T}_{diag})}_{\text{interactions}} \underbrace{(I + \tilde{G}_{diag}K)}_{\text{individual loops}}$$

ETC.....

(quite a lot of theory available, RGA etc.)

Conclusions / Future work

1. Control structure design: Issues must be defined
2. Tools and theory are developing; Controllability analysis
3. Use feedback effectively - feedback hierarchies
4. Balance between centralized and cascade/decentralized implementations
5. Balance between complexity and performance
6. Balance between modelling effort and performance
7. Mathematical problem formulation is difficult (non-convex):
 - Optimal design of K with given no. of non-zero elements
 - Penalize links and controller complexity
 - Controllability analysis approaches; branch and bound

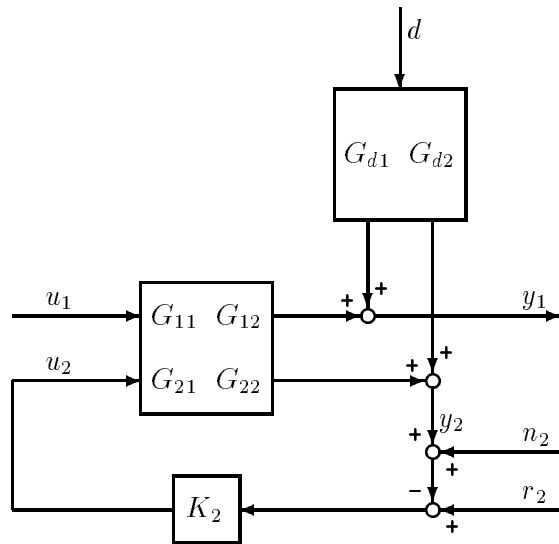


Figure 1: Block diagram of a partial control system