

Simulation of Subsurface Two-Phase Flow in an Oil Reservoir

Carsten Völcker, John Bagterp Jørgensen, Per Grove Thomsen and Erling Halfdan Stenby

*Technical University of Denmark (DTU)
Department of Informatics and Mathematical Modeling (IMM)*

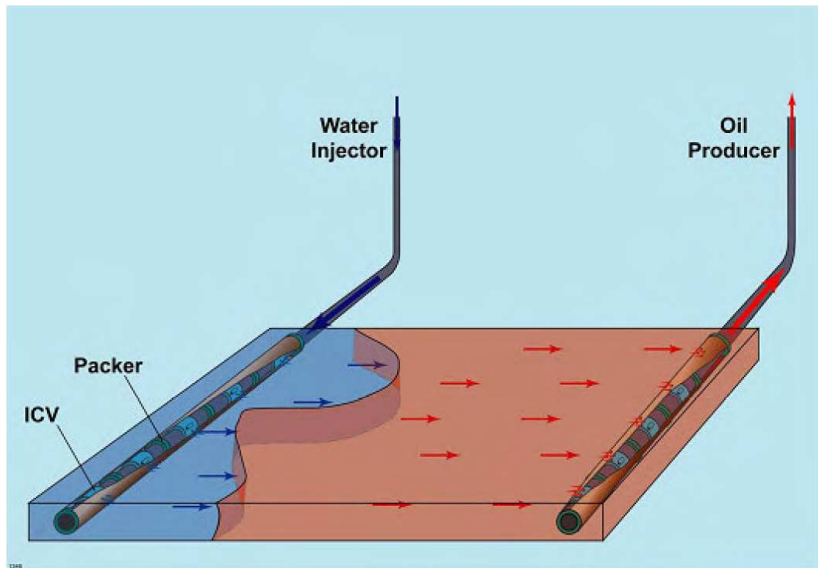
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 - Conservation Equations
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- 3 Numerical Integration
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- 4 Solving The Linear Equations
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2D Reservoir



Optimizing Production

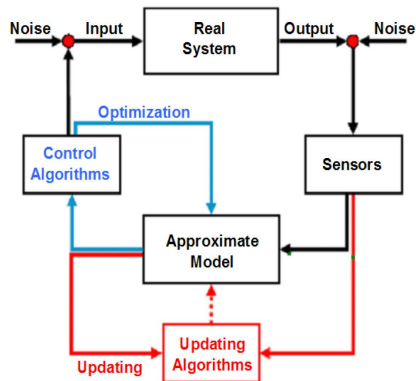
Maximizing net present value (NPV):

$$\max_u \text{NPV} = \int_{t_0}^t l(x(t), u) dt$$

$$\text{s.t.} \quad \frac{d}{dt} g(x(t)) = f(x(t), u)$$

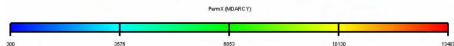
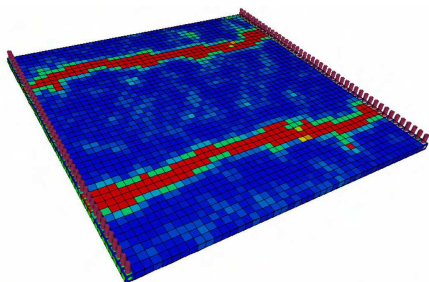
$$x(t_0) = x_0$$

Closed loop optimizer:

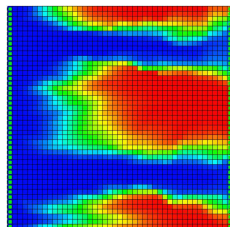


Water Flooding without/with Optimal Control

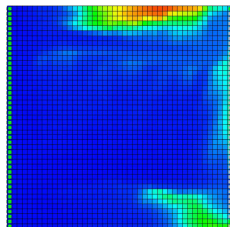
Permeability field with two streaks:



Without optimal control:



With optimal control:



Conservation Equations

Mass conservation of water and oil:

$$\frac{\partial}{\partial t} C_w(P_w, S_w) = -\nabla N_w(P_w, S_w) + Q_w$$

$$\frac{\partial}{\partial t} C_o(P_o, S_o) = -\nabla N_o(P_o, S_o) + Q_o$$

- No flow potential due to gravitation.
- Homogenous permeability field.
- Capillary pressure neglected.
- Incompressible rock.

Mass concentrations:

$$C_w = \phi \rho_w(P_w) S_w$$

$$C_o = \phi \rho_o(P_o) S_o$$

Fluxes through the porous medium:

$$N_w = \rho_w(P_w) u_w(P_w, S_w)$$

$$N_o = \rho_o(P_o) u_o(P_o, S_o)$$

Darcy Velocity and Boundary Conditions

Pressure driven flow, Darcy's law:

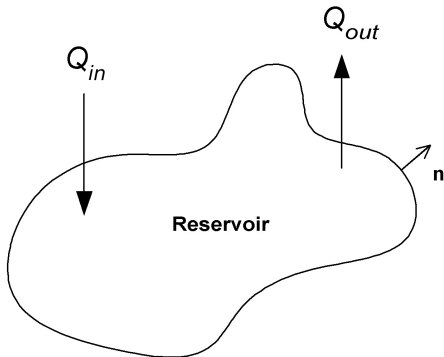
$$u_{\alpha} = -\mathbf{k} \frac{k_{r\alpha}(S_{\alpha})}{\mu_{\alpha}} \nabla P_{\alpha} \quad \alpha = o, w$$

No flow across boundaries:

$$\mathbf{u}_{\alpha} \cdot \mathbf{n} = 0 \quad \text{and} \quad \mathbf{u}_{\alpha} \cdot \mathbf{n} = 0$$

Internal sources/sinks due to wells:

- Water is injected to maintain pressure and replace the oil.
- Oil and water are produced.



Reduction Of State Variables:

Water saturation (volume fraction):

$$S_w + S_o = 1$$

Pressure difference due to capillary pressure:

$$P_{cow} = P_o - P_w$$

Reduction of variables:

$$S_w = 1 - S_o \quad \Rightarrow \quad S = S_w = 1 - S_o$$

$$P_{cow} = 0 \quad \Rightarrow \quad P = P_w = P_o$$

State variables $(S, P) = (S_w, P_o)$:

$$S = S(t, s)$$

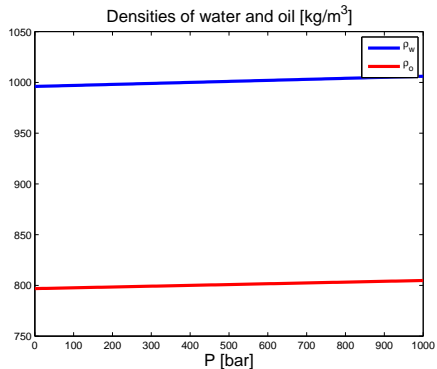
$$P = P(t, s)$$

Density and compressibility

Compressible fluids:

$$\rho_w = \rho_{w0} e^{P - P_{w0}}$$

$$\rho_o = \rho_{o0} e^{P - P_{o0}}$$



Relative Permeabilities by The Corey Relations

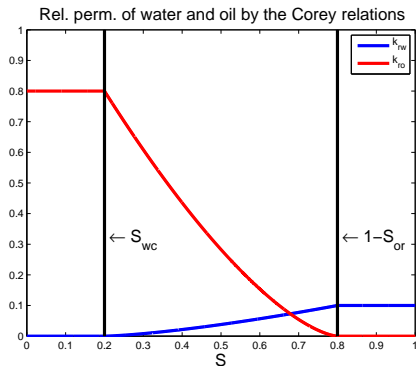
Relative permeabilities:

$$k_{rw} = k_{rw0} s^{n_w}$$

$$k_{ro} = k_{ro0} (1 - s)^{n_w}$$

Reduced water saturation:

$$s = \frac{S - S_{wc}}{1 - S_{wc} - S_{or}}$$



Different Formulation

Partial differential equation (PDE) model:

$$\begin{aligned}\frac{\partial}{\partial t}C_w(P_w, S_w) &= -\nabla N_w(P_w, S_w) + Q_w \\ \frac{\partial}{\partial t}C_o(P_o, S_o) &= -\nabla N_o(P_o, S_o) + Q_o\end{aligned}$$

Different formulation of an ordinary differential equation (ODE) model after discretizing spatially:

$$\frac{d}{dt}g(x(t)) = f(t, x(t)) \quad x(t_0) = x_0$$

Runge-Kutta Methods

Tailored formulation of an s -stage Runge-Kutta method:

$$T_i = t_n + c_i h_n \quad i = 1, 2, \dots, s$$

$$g(X_i) = g(x_n) + h_n \sum_{j=1}^s a_{ij} f(T_j, X_j) \quad i = 1, 2, \dots, s$$

$$g(x_{n+1}) = g(x_n) + h_n \sum_{j=1}^s b_j f(T_j, X_j)$$

$$g(\hat{x}_{n+1}) = g(x_n) + h_n \sum_{j=1}^s \hat{b}_j f(T_j, X_j)$$

$$e_{n+1} = g(x_{n+1}) - g(\hat{x}_{n+1}) = h_n \sum_{j=1}^s d_j f(T_j, X_j) \quad d_j = b_j - \hat{b}_j$$

Fast Integration by ESDIRK

Only $s - 1$ implicit stages:

0	0				
c_2	a_{21}	γ			
c_3	a_{31}	a_{32}	γ		
\vdots	\vdots			\ddots	
1	b_1	b_2	b_3	\dots	γ
	b_1	b_2	b_3	\dots	γ
	\hat{b}_1	\hat{b}_2	\hat{b}_3	\dots	\hat{b}_s
	d_1	d_2	d_3	\dots	d_s



ERK



DIRK



SDIRK



ESDIRK



FIRK

Modified Newton Step

The state values X_i are obtained by sequential solution of the residual:

$$R(X_i) = g(X_i) - h_n \gamma f(T_i, X_i) - \psi_i = 0 \quad i = 2, 3, \dots, s$$

$$\psi_i = g(x_n) + h_n \sum_{j=1}^{i-1} a_{ij} f(T_j, X_j) \quad i = 2, 3, \dots, s$$

The Jacobian of the residual $R(X_i)$:

$$\begin{aligned} J(X_i) &= \frac{\partial R}{\partial X_i}(X_i) = \frac{\partial g}{\partial x}(X_i) - h_n \gamma \frac{\partial f}{\partial x}(T_i, X_i) \\ &\approx \frac{\partial g}{\partial x}(x_m) - h_m \gamma \frac{\partial f}{\partial x}(t_m, x_m) \\ &= J(x_m) = LU \end{aligned}$$

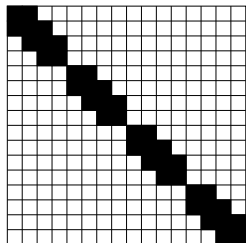
Only updating the Jacobian by slow convergence or divergence:

$$LU \Delta X_i = R(X_i)$$

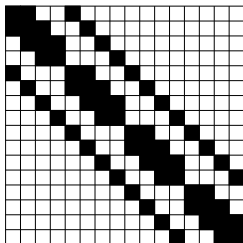
$$X_i := X_i - \Delta X_i$$

Jacobian Structure

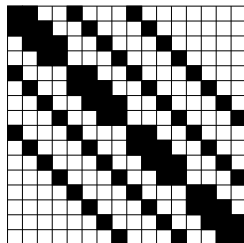
1D: 3 Non-zeros:



2D: 5 Non-zeros:



3D: 7 Non-zeros:



Solving the linear equations:

- Sparse direct solver: LU factorization and back substitution.
- Iterative solver: GMRES.

Adaptive Time Stepping

In most commercial simulators:

- Simple heuristics implemented e.g. maximum variation of saturations.

ESDIRK, embedded error estimator:

$$\hat{e}_{n+1} = g(x_{n+1}) - g(\hat{x}_{n+1}) = h_n \sum_{i=1}^s d_i f(T_i, X_i)$$

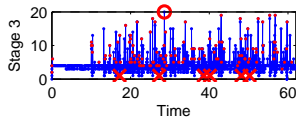
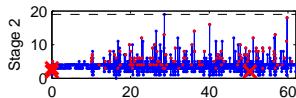
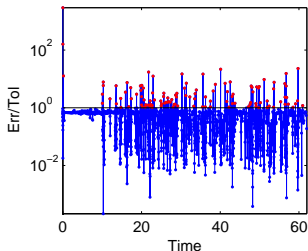
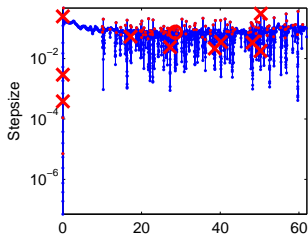
Measures of the error may be controlled adjusting the time step according to

$$h_{n+1} = \frac{h_n}{h_{n-1}} \left(\frac{\varepsilon}{\hat{r}_{n+1}} \right)^{k_2/k} \left(\frac{\hat{r}_n}{\hat{r}_{n+1}} \right)^{k_1/k} h_n$$

- \hat{e}_{n+1} is an error estimate of the conserved quantities $g(x_{n+1})$.

ESDIRK Performance

ESDIRK23 performance and statistics, 45×45 grid blocks:

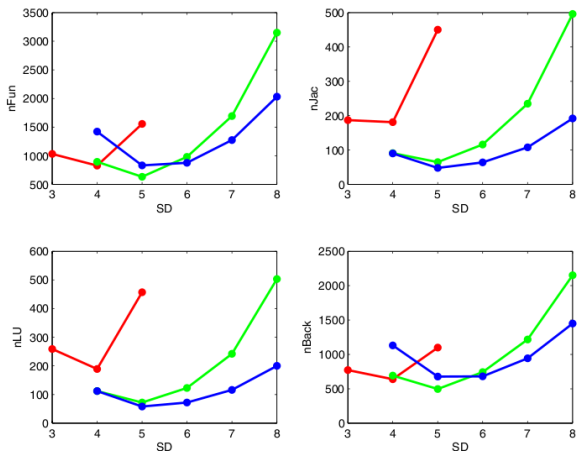


Method : ESDIRK23 nIter 2 : 4734
 absTol : 4050x1 nIter 3 : 5506
 relTol : 4050x1

nStep : 1289 nFun : 12815
 nFail : 129 nJac : 1279
 nDiv : 10 nLU : 1290
 nSlow : 1 nBack : 10240

Performance by Significant Digits

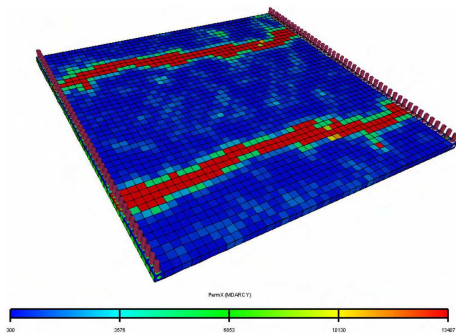
ESDIRK performance on 1D case, 1000 grid blocks:



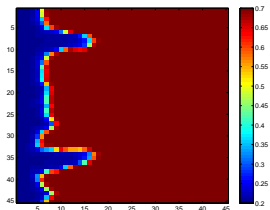
● ESDIRK12 = red, ESDIRK23 = green, ESDIRK34 = blue.

2D Test Case, 45×45 Grid Blocks

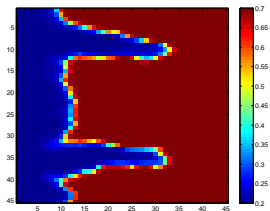
Permeability field with two streaks:



Oil saturation after 31 days:



Oil saturation after 62 days:



Butcher Tableau's of Runge-Kutta Methods

The explicit Runge-Kutta (ERK) method:

0	0				
c_2	a_{21}	0			
c_3	a_{31}	a_{32}	0		
\vdots	\vdots			\ddots	
c_s	a_{s1}	a_{s2}	a_{s3}	\cdots	0
	b_1	b_2	b_3	\cdots	b_s
	\hat{b}_1	\hat{b}_2	\hat{b}_3	\cdots	\hat{b}_s
	d_1	d_2	d_3	\cdots	d_s

The A-matrix in Runge-Kutta methods:



ERK

Butcher Tableau's of Runge-Kutta Methods

The diagonally implicit Runge-Kutta (DIRK) method:

c_1	a_{11}				
c_2	a_{21}	a_{22}			
c_3	a_{31}	a_{32}	a_{33}		
\vdots	\vdots			\ddots	
c_s	a_{s1}	a_{s2}	a_{s3}	\cdots	a_{ss}
	b_1	b_2	b_3	\cdots	b_s
	\hat{b}_1	\hat{b}_2	\hat{b}_3	\cdots	\hat{b}_s
	d_1	d_2	d_3	\cdots	d_s

The A-matrix in Runge-Kutta methods:



ERK



DIRK

Butcher Tableau's of Runge-Kutta Methods

The singly diagonally implicit Runge-Kutta (SDIRK) method:

c_1	γ				
c_2	a_{21}	γ			
c_3	a_{31}	a_{32}	γ		
\vdots	\vdots			\ddots	
c_s	a_{s1}	a_{s2}	a_{s3}	\cdots	γ
	b_1	b_2	b_3	\cdots	b_s
	\hat{b}_1	\hat{b}_2	\hat{b}_3	\cdots	\hat{b}_s
	d_1	d_2	d_3	\cdots	d_s

The A-matrix in Runge-Kutta methods:



ERK



DIRK



SDIRK

Butcher Tableau's of Runge-Kutta Methods

The explicit singly diagonally implicit Runge-Kutta (ESDIRK) method:

$$\begin{array}{c|cccc}
 0 & 0 & & & \\
 c_2 & a_{21} & \gamma & & \\
 c_3 & a_{31} & a_{32} & \gamma & \\
 \vdots & \vdots & & & \ddots \\
 c_s & a_{s1} & a_{s2} & a_{s2} & \cdots & \gamma \\
 \hline
 & b_1 & b_2 & b_3 & \cdots & b_s \\
 & \hat{b}_1 & \hat{b}_2 & \hat{b}_3 & \cdots & \hat{b}_s \\
 \hline
 & d_1 & d_2 & d_3 & \cdots & d_s
 \end{array}$$

The A-matrix in Runge-Kutta methods:



ERK



DIRK



SDIRK



ESDIRK

Butcher Tableau's of Runge-Kutta Methods

The fully implicit Runge-Kutta (FIRK) method:

c_1	a_{11}	a_{12}	a_{13}	\cdots	a_{1s}
c_2	a_{21}	a_{22}	a_{23}		a_{2s}
c_3	a_{31}	a_{32}	a_{33}		a_{3s}
\vdots	\vdots			\ddots	\vdots
c_s	a_{s1}	a_{s2}	a_{s3}	\cdots	a_{ss}
	b_1	b_2	b_3	\cdots	b_s
	\hat{b}_1	\hat{b}_2	\hat{b}_3	\cdots	\hat{b}_s
	d_1	d_2	d_3	\cdots	d_s

The A-matrix in Runge-Kutta methods:



ERK



DIRK



SDIRK



ESDIRK



FIRK

Fast Integration by ESDIRK

Only $s - 1$ implicit stages:

0	0				
c_2	a_{21}	γ			
c_3	a_{31}	a_{32}	γ		
\vdots	\vdots			\ddots	
1	b_1	b_2	b_3	\cdots	γ
	b_1	b_2	b_3	\cdots	γ
	\hat{b}_1	\hat{b}_2	\hat{b}_3	\cdots	\hat{b}_s
	d_1	d_2	d_3	\cdots	d_s



ESDIRK

Fast Integration by ESDIRK

Only $s - 1$ implicit stages:

0	0				
c_2	a_{21}	γ			
c_3	a_{31}	a_{32}	γ		
\vdots	\vdots			\ddots	
1	b_1	b_2	b_3	\cdots	γ
	b_1	b_2	b_3	\cdots	γ
	\hat{b}_1	\hat{b}_2	\hat{b}_3	\cdots	\hat{b}_s
	d_1	d_2	d_3	\cdots	d_s

The first stage is explicit, which implies that:

$$X_1 = x_n$$

$$x_{n+1} = X_s$$

Fast Integration by ESDIRK

Only $s - 1$ implicit stages:

0	0					
c_2	a_{21}	γ				
c_3	a_{31}	a_{32}	γ			
\vdots	\vdots			\ddots		
1	b_1	b_2	b_3	\cdots	γ	
	b_1	b_2	b_3	\cdots	γ	
	\hat{b}_1	\hat{b}_2	\hat{b}_3	\cdots	\hat{b}_s	
	d_1	d_2	d_3	\cdots	d_s	

The Butcher tableau is constructed such that:

$$X_1 = x_n$$

$$x_{n+1} = X_s$$

Fast Integration by ESDIRK

Only $s - 1$ implicit stages:

0	0				
c_2	a_{21}	γ			
c_3	a_{31}	a_{32}	γ		
\vdots	\vdots			\ddots	
1	b_1	b_2	b_3	\cdots	γ
	b_1	b_2	b_3	\cdots	γ
	\hat{b}_1	\hat{b}_2	\hat{b}_3	\cdots	\hat{b}_s
	d_1	d_2	d_3	\cdots	d_s

The state values X_i are obtained by sequential solution of the residual:

$$R(X_i) = g(X_i) - h_n \gamma f(T_i, X_i) - \psi_i = 0 \quad i = 2, 3, \dots, s$$

$$\psi_i = g(x_n) + h_n \sum_{j=1}^{i-1} a_{ij} f(T_j, X_j) \quad i = 2, 3, \dots, s$$