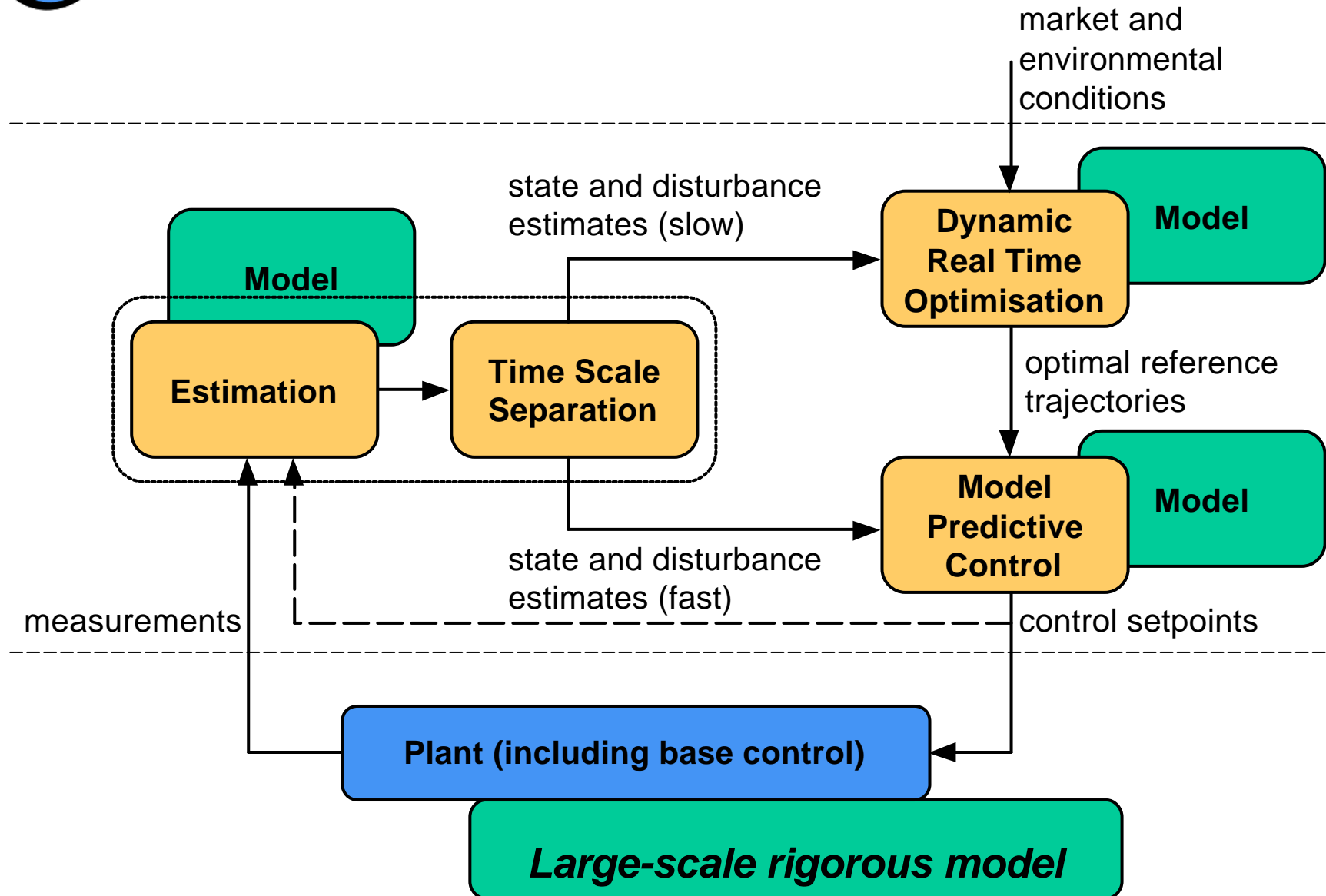
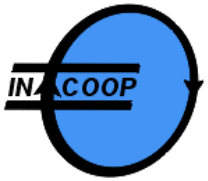


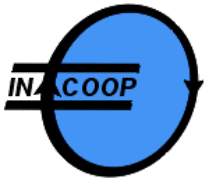
# Hybrid modelling and model reduction for control & optimisation

based on research done by  
RWTH-Aachen and TU Delft

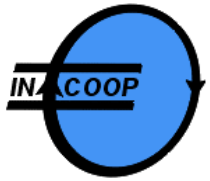
presented by Johan Grievink

**INCOOP Workshop**  
Düsseldorf, 23-24 January, 2003










- \* Large scale physical modeling
- \* Hybrid components
- \* Physical based complexity reduction
- \* Mathematical complexity reduction
- \* Application aspects for INCOOP tasks
- \* Conclusions

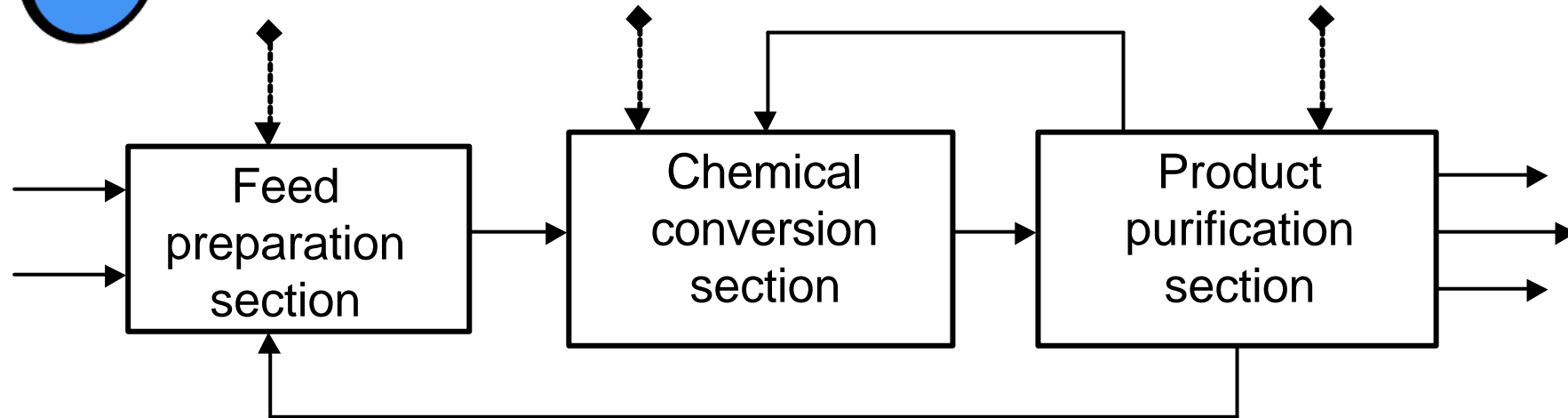
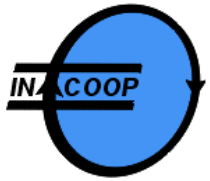


## Plant operations modelling:

- *process with sensors and actuators* 
- *conventional controllers* 
- *external disturbances* 
- operating window constraints -
- economical objectives -

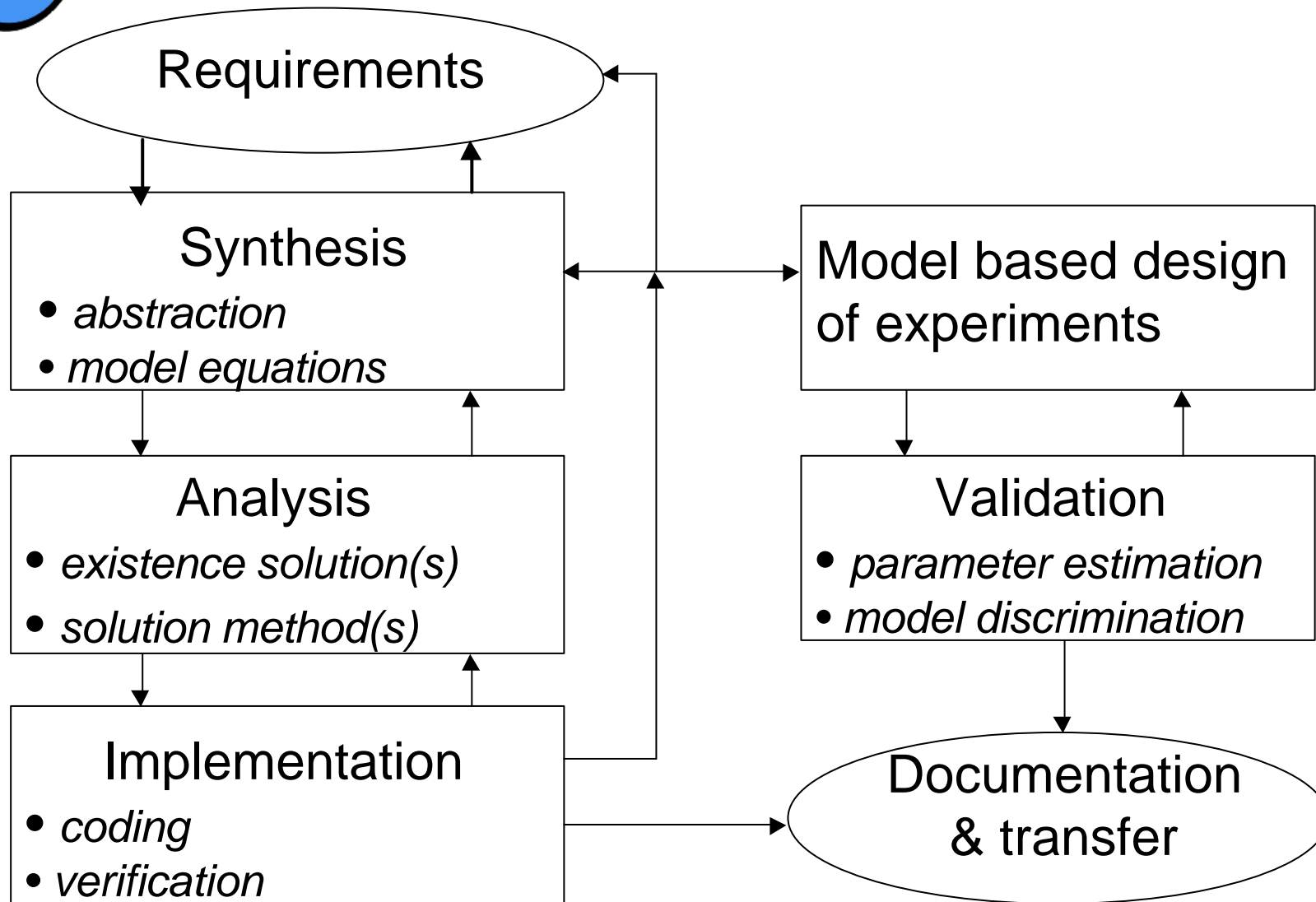
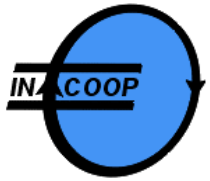
## Aspects of modelling:

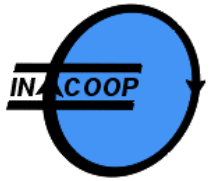
- *technology of modelling* 
- mainly generic aspects 
- specific aspects: see Bayer and Shell applications
- work processes underexposed



- multiple modes of production + switching
- disturbances
- multiple units / section & many compartments / unit
- recycling & heat integration
- non-linear behaviour (units + plant wide integration)
- very wide range of relevant time scales ( $\mu\text{s}$  - days)
- several thermodynamic phases with many species

=> Large scale dynamic process models ( $10^3$  -  $10^5$  DAE's)



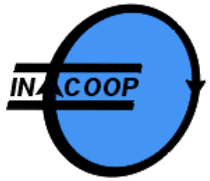


Aim: accurate representation of physical behaviour:

- *relevant time scales*                      => how small ?
- *feasible operational window:*
  - \* *physical ranges of inputs, states, outputs*
- *for realistic disturbance scenarios*

Trade-off's:

- *complexity vs costs of development & validation*
- *complexity vs maintenance (costs)*
- *in closed loop: complexity vs accuracy*



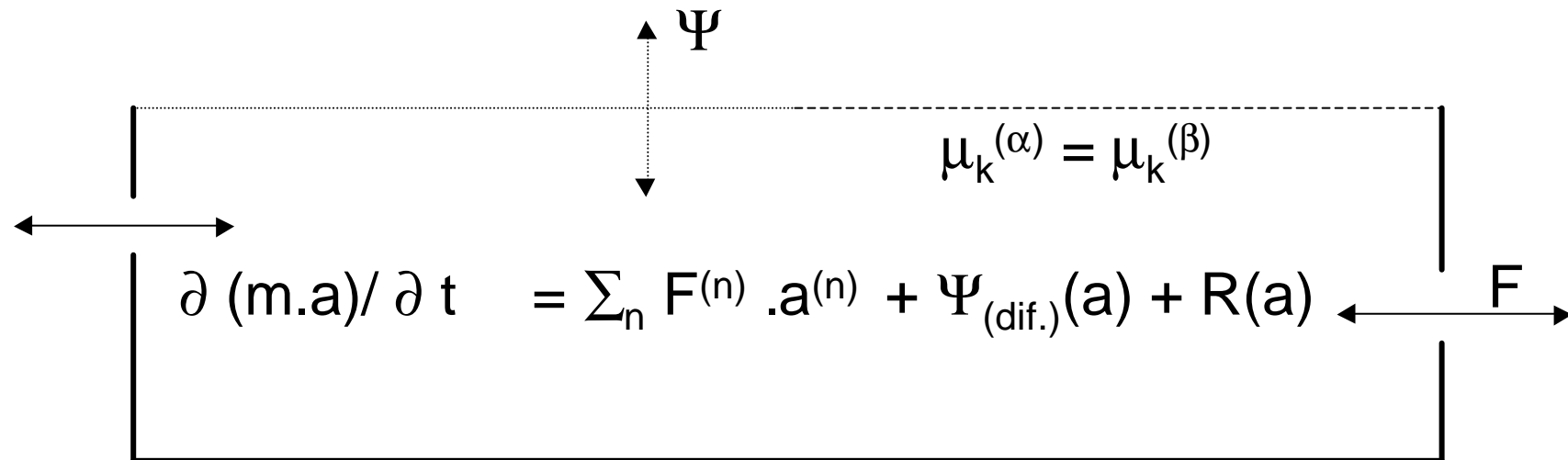
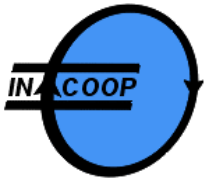
Abstraction:

from reality to a modelling space with bounds:

- objects: *contents and walls of equipment, streams, sensors, controllers, actuators, ..*
- spatial resolution: *mixed compartments, distributed in n-D.*
- time resolution: *continuous, discrete*
- chemical species: *discrete, continuous*
- thermodynamic phases: *V, L<sub>1</sub>, L<sub>2</sub>, S<sub>1</sub>, S<sub>2</sub>, ..*
- chemical reactions: *discrete, continuous;*
- states of particles: *size, stress, charge, ..*
- .....

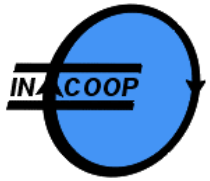
Key issue: how to find relevant level of detail





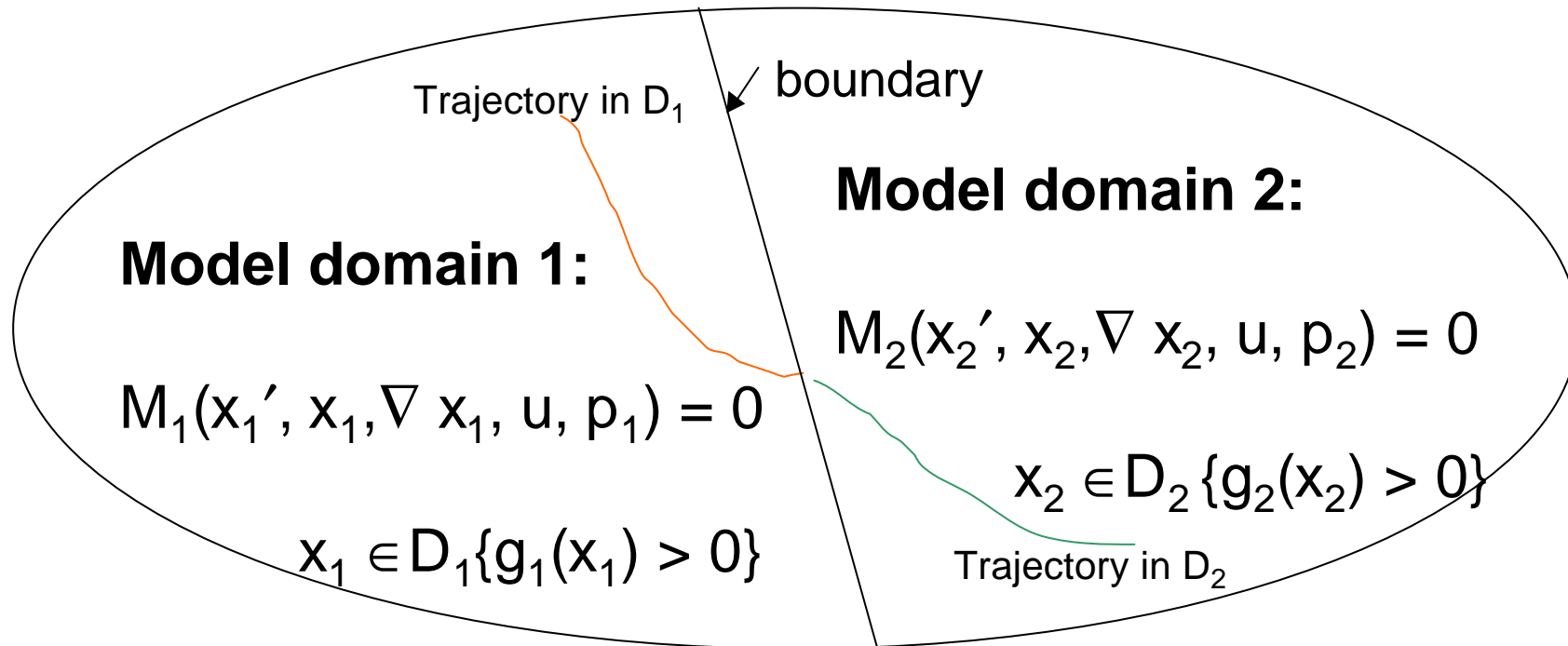
Model equations:

- conservation / change: *truly first principles*
- thermodynamic states:  $a=a(P,T,c)$
- transfer rate:  $\Psi = \Psi(\nabla P, \nabla T, \nabla c), F=F(\nabla P)$
- source/sink rates:  $R=R(P,T,c)$
- phase equilibria:  $\mathbf{m}_k^{(a)} = \mathbf{m}_k^{(b)}, T^{(a)} = T^{(b)}$



Equations for:

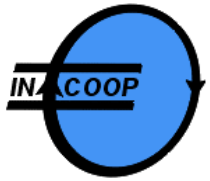
- thermodynamic variables per species and per phase:  
density, specific heat, entropy, enthalpy, free enthalpy
- transport coefficients:  
viscosity, heat diffusion, species diffusion, surface tension
- Needed information:  
variables:  $P_k(p_k^{(0)}, P, T; \text{par}_k) = 0$       and       $p^{(\alpha)} = P^{(\alpha)}(P, T, x, p^{(0)})$   
gradients:  $\partial p / \partial q = \partial P(P, T, x) / \partial q$       with  $q = \{ P, T, x \}$
- Issues:  
models in “closed” software box  
computational speed & accuracy of solution ?



Transition: *e.g. phase split*

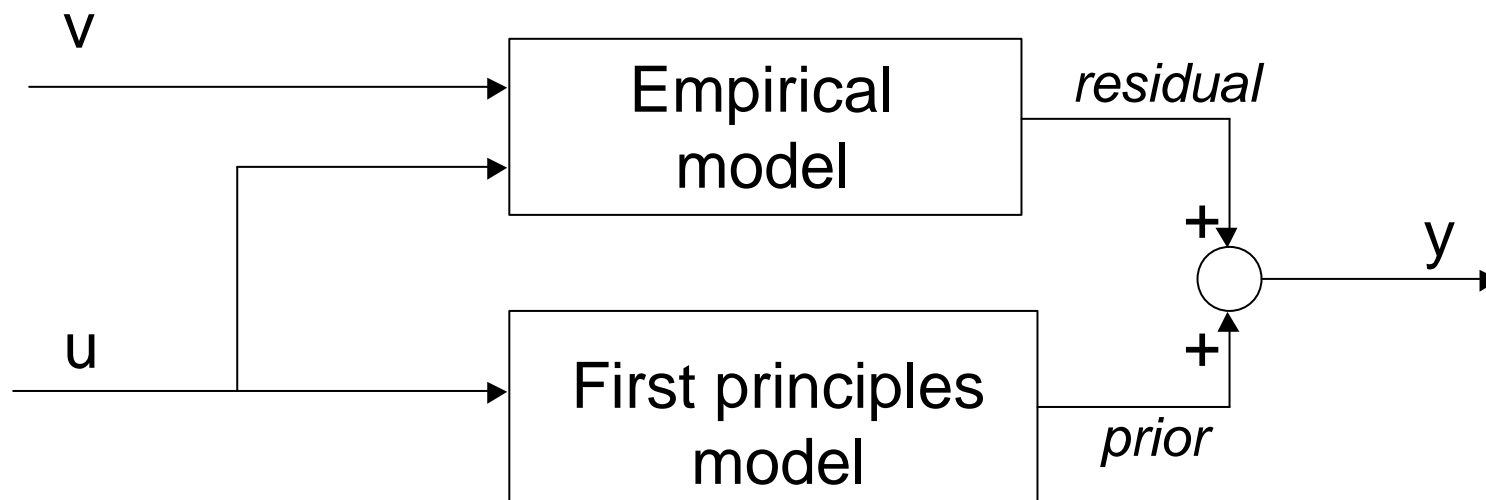
State event:  $g_1(x_1) = 0$  if approaching from  $D_1$   
 $g_2(x_2) = 0$  if approaching from  $D_2$

Continuity:  $T(x_1, \nabla x_1, x_2, \nabla x_2, ) = 0$

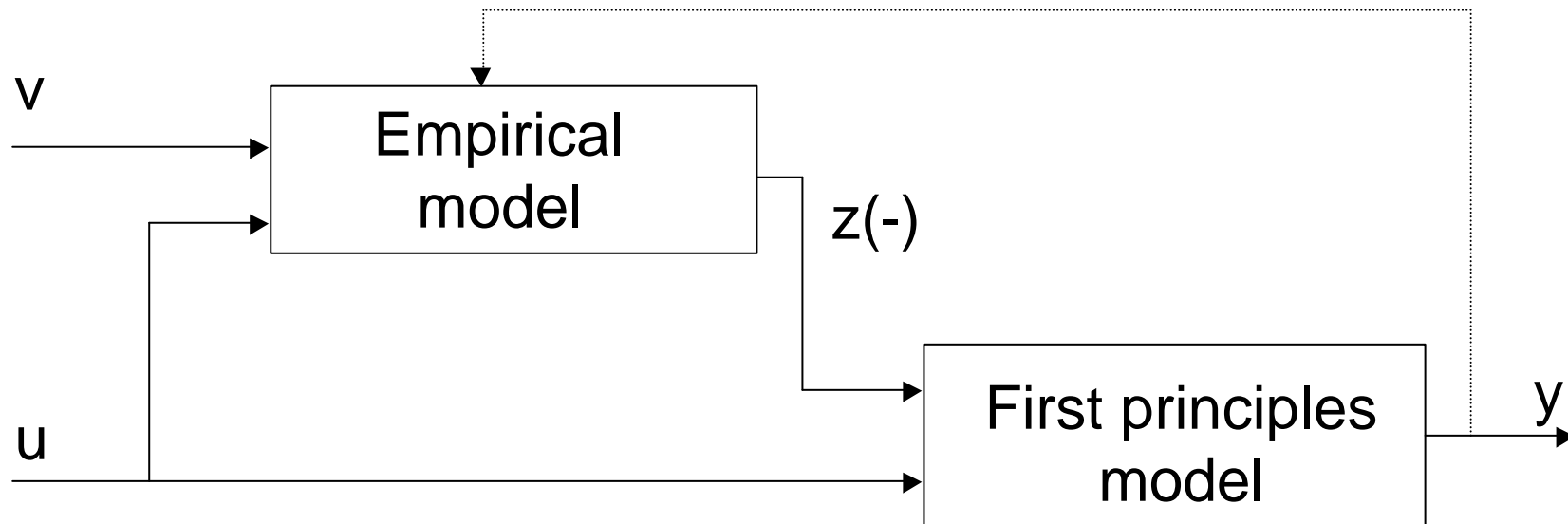


Hybrid models comprise first principles as well as empirical components to deal with uncertainty or complexity.

Parallel structure: ad-hoc model error compensation

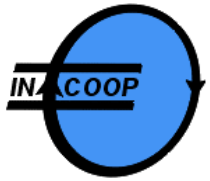


Sequential structure: physically motivated extension



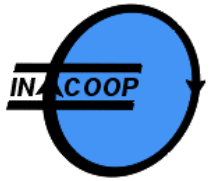
Empirical modelling:

- static (non-linear) regression model; e.g. ANN,  $z = z(\pi, v, u, y)$
- dynamic trend model:  $z(t) = z(\pi, v, u, y)$  with  $\pi' = 0$ ; update of  $\pi$



Requirements to empirical components in combination with physical modelling:

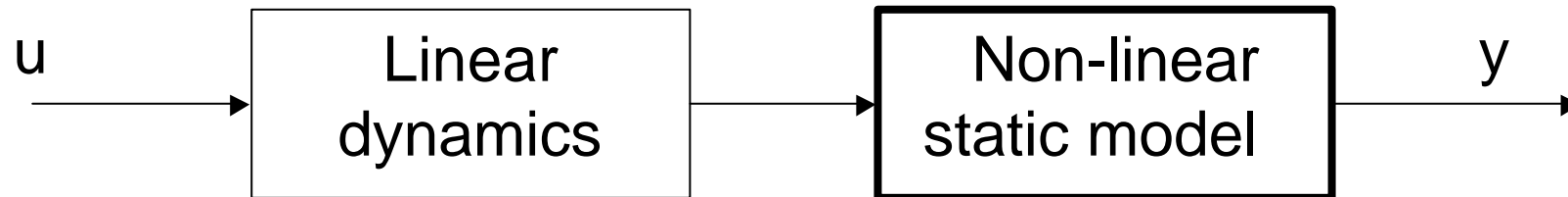
- continuous and differentiable (bounded) in all variables
- comply with correct physical asymptotic behaviour:
  - $\partial x / \partial t, \nabla x \geq 0$  for  $x \downarrow 0$  when  $x \geq 0$ ; e.g. **not**  $dc / dt = k \cdot c^{-a}$  ( $a > 0$ );
  - no fluxes remain when forces vanish; equilibrium conditions
- no introduction of spurious roots
  - e.g. rate =  $k_1 \cdot c / (1 + k_2 \cdot c + k_3 \cdot c^2)$
  - second order term in denominator may enhance fitting accuracy but it creates a maximum in the rate, allowing for multiple solutions.



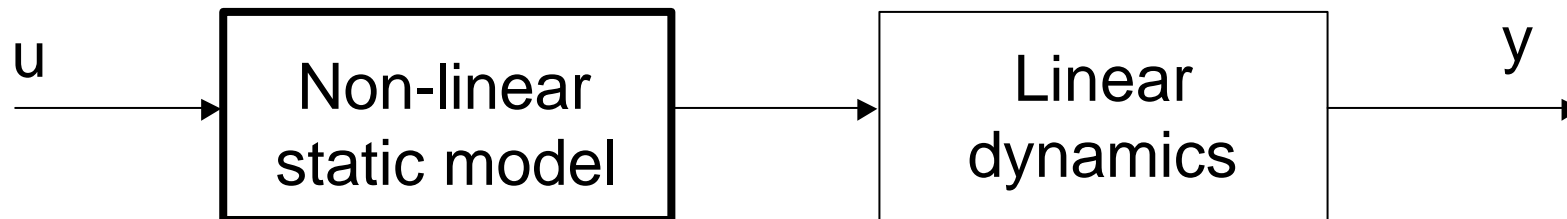
# LSM: Wiener / Hammerstein hybrid models **TU Delft**

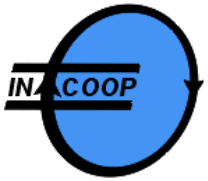
- static fundamental model available (process simulators)
- plant dynamics accessible by plant tests (linear models)

*Wiener* structure:



*Hammerstein* structure:





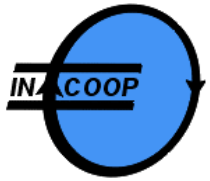
Connectivity conditions:  $f \equiv y_1 - y_2 = 0$

Physical consequences of coupling (mass / heat):

- *recycles increase I/O time constants:  $T = \sum_i \tau_i / (1 - \prod_i K_i)$*
- *can induce non-linear, positive feedback:*

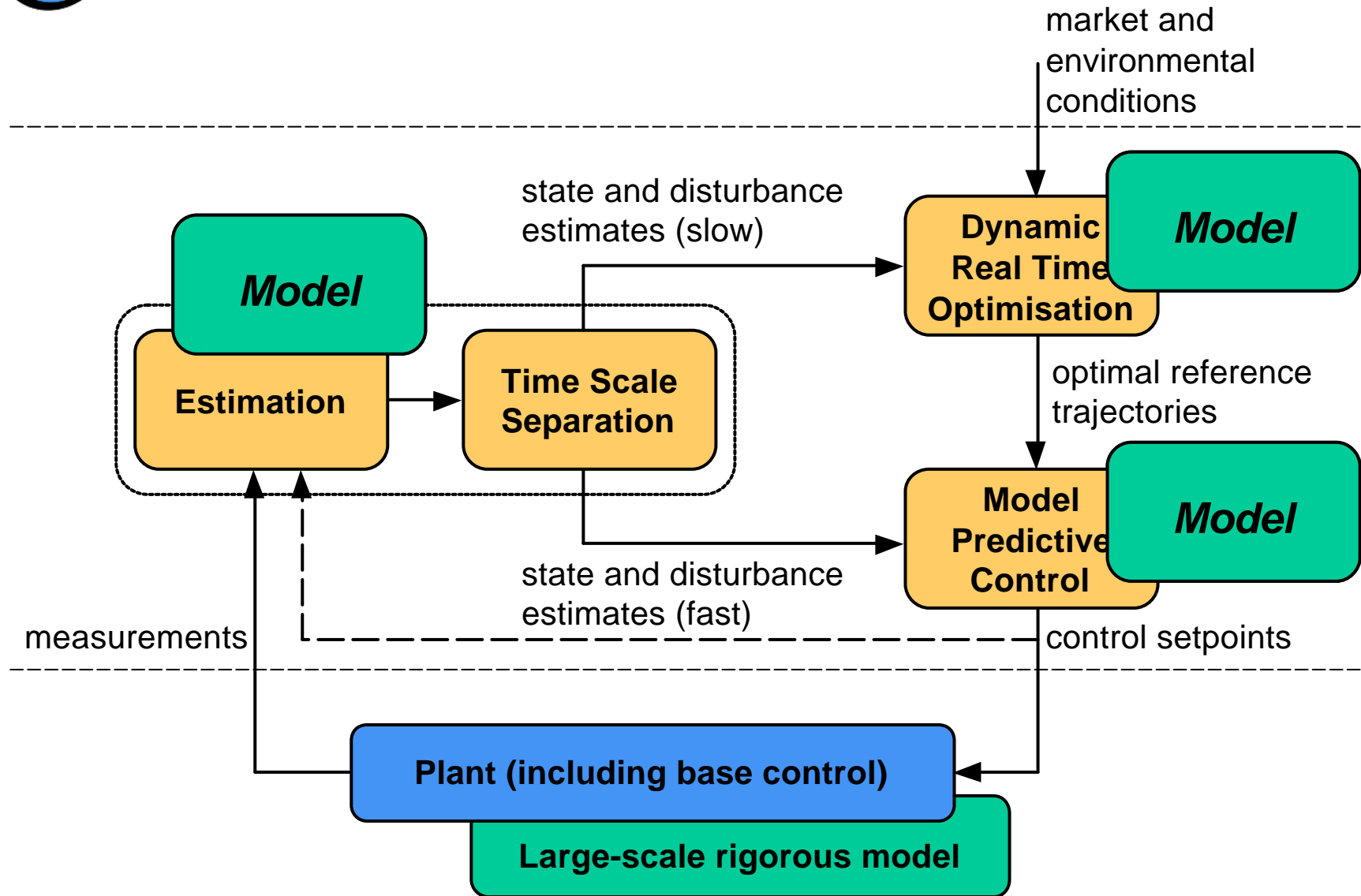
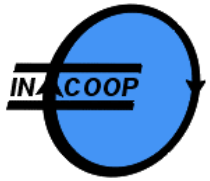
=> multiple stationary states can occur

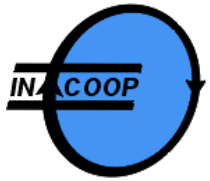




- Focus has been on model synthesis
- Structured approach is essential to reduce modelling errors
- Decomposition / aggregation at the finer scales ?
- Model synthesis more an art than a science
  
- Not covered: many other important aspects
  - *differential index problems*
  - *scaling and initialisations of DAE's*
  - *global sensitivity analysis*
  - *experimental validation aspects*

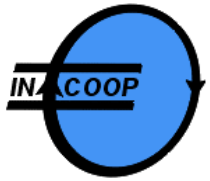
Large scale plant model will now serve as 'source' model for reduction to models suitable for on-line use in control and optimisations





## Options for reduction:

- reduce the modelling space
  - lumping of species, reactions, phases
  - combining compartments, lumping by OCFE
  - ...
- simplify equations (structure):
  - by linearisation;
  - (non-linear) approximations of complex expressions;  
e.g for physical properties and kinetics
- reduce number of equations / order reduction
  - remove trivial linear connectivity equations and variables
  - order reduction



## Modular modeling (e.g. in gPROMS)

- ⇒ large number of redundant equations of type  $X = Y$   
(e.g. connection of different trays in distillation column)
- ⇒ increased model size without additional physical information

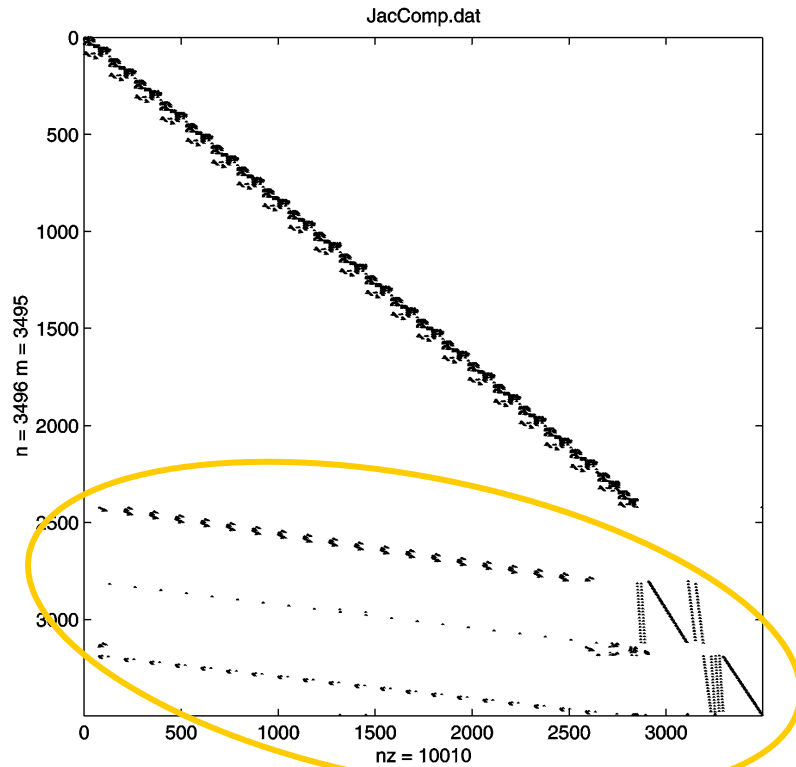
### Idea:

- ⇒ Determine redundant equations and variables by automatic analysis of the system's incident matrix
- ⇒ Perform automatic mapping of variables in simulation / optimization software

### Prototype

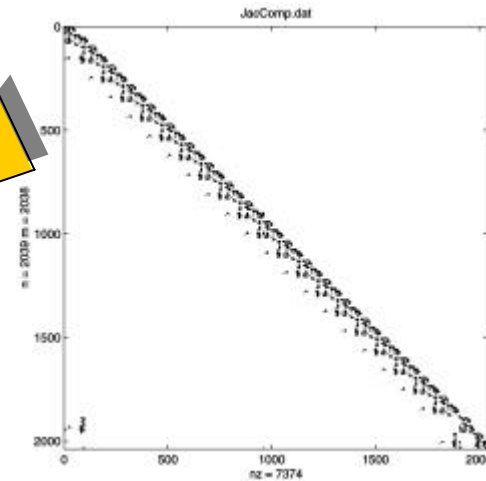
- ⇒ Implemented in sequential approach dynamic optimization software

## Application to distillation column I

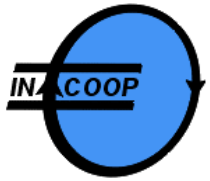


Redundant equations

Simplification procedure



- Model size reduced from 3496 to 2039
- Computation time in optimization reduced by 53%



Singular perturbation:

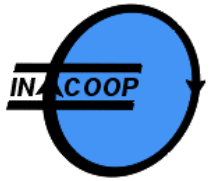
$$\dot{x}_2 = 0$$

$$\begin{aligned} \dot{x}_1 &= f_1(x_1, x_2, u) \\ \dot{x}_2 &= f_2(x_1, x_2, u) \end{aligned} \quad \Rightarrow \quad \begin{aligned} \dot{x}_1 &= f_1(x_1, x_2, u) \\ 0 &= f_2(x_1, x_2, u) \end{aligned}$$

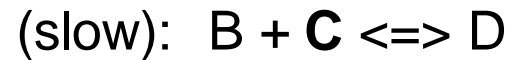
Truncation:

$$x_2 = c$$

$$\begin{aligned} \dot{x}_1 &= f_1(x_1, x_2, u) \\ \dot{x}_2 &= f_2(x_1, x_2, u) \end{aligned} \quad \Rightarrow \quad \begin{aligned} \dot{x}_1 &= f_1(x_1, c, u) \\ c &= x_2 \end{aligned}$$



Batch reactions:



Model:

$$\begin{aligned}c_A' &= -r_2 & r_1 &= k_1(c_B \cdot c_C - c_D / K_1) \\c_B' &= -r_1 + r_2 & r_2 &= k_2(c_A \cdot c_D - c_B \cdot c_E / K_2) \\c_C' &= -r_1 & k_2 &= k_1 / e \\c_D' &= +r_1 - r_2 \\c_E' &= +r_2\end{aligned}$$

**Transform** model to separate fast and slow modes

$$\xi_1' = r_1$$

$$\xi_2' = r_2 \Rightarrow e. \xi_2' = \underline{r}_2$$

$$c_A = c_A^0 - \xi_2$$

$$c_B = c_B^0 - \xi_1 + \xi_2$$

$$c_C = c_C^0 - \xi_1$$

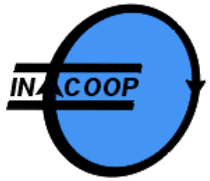
$$c_D = c_D^0 + \xi_1 - \xi_2$$

$$c_E = c_E^0 + \xi_2$$

**Singular perturbation:**

$$\xi_1' = r_1(\xi_1, \xi_2)$$

$$0 = r_2(\xi_1, \xi_2)$$



## Generic procedure

1. Transform original state space into a state space better revealing important process dynamics

$$x - x^* = Uz$$

2. Decomposition into two complementary subspaces

$$Uz = U_1 z_1 + U_2 z_2, \quad U = [U_1, U_2]$$

Substitution into original DAE system and decomposition yields

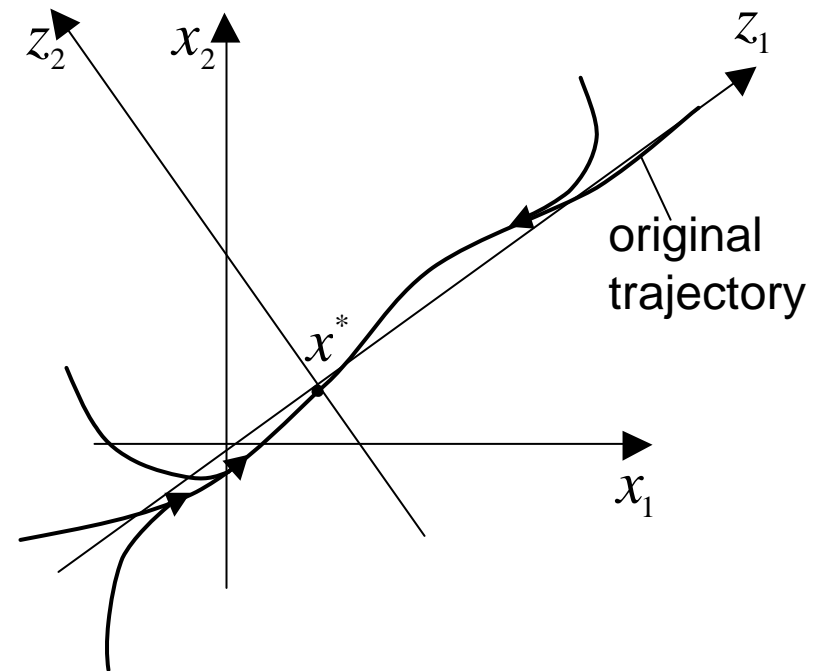
$$\dot{z}_1 = U_1^T f(x^* + U_1 z_1 + U_2 z_2, y, u)$$

$$\dot{z}_2 = U_2^T f(x^* + U_1 z_1 + U_2 z_2, y, u)$$

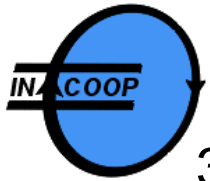
$$z_1(0) = U_1^T (x_0 - x^*)$$

$$z_2(0) = U_2^T (x_0 - x^*)$$

$$0 = g(x^* + U_1 z_1 + U_2 z_2, y, u)$$







### 3. Deduction of a reduced model

#### a) Truncation ( $z_2 = 0$ )

$$\dot{z}_1 = U_1^T f(x^* + U_1 z_1, y, u)$$

$$z_1(0) = U_1^T (x_0 - x^*)$$

$$0 = g(x^* + U_1 z_1, y, u)$$

- lower number of equations and variables than original model
- not steady-state accurate

#### b) Residualization ( $\dot{z}_2 = 0$ )

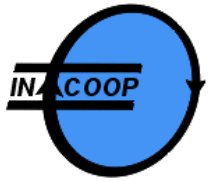
$$\dot{z}_1 = U_1^T f(x^* + U_1 z_1 + U_2 z_2, y, u)$$

$$0 = U_2^T f(x^* + U_1 z_1 + U_2 z_2, y, u)$$

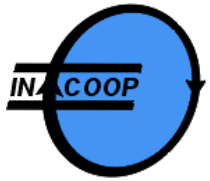
$$z_1(0) = U_1^T (x_0 - x^*)$$

$$0 = g(x^* + U_1 z_1 + U_2 z_2, y, u)$$

- same size as original model, but less differential and more algebraic equations and variables
- steady-state accurate



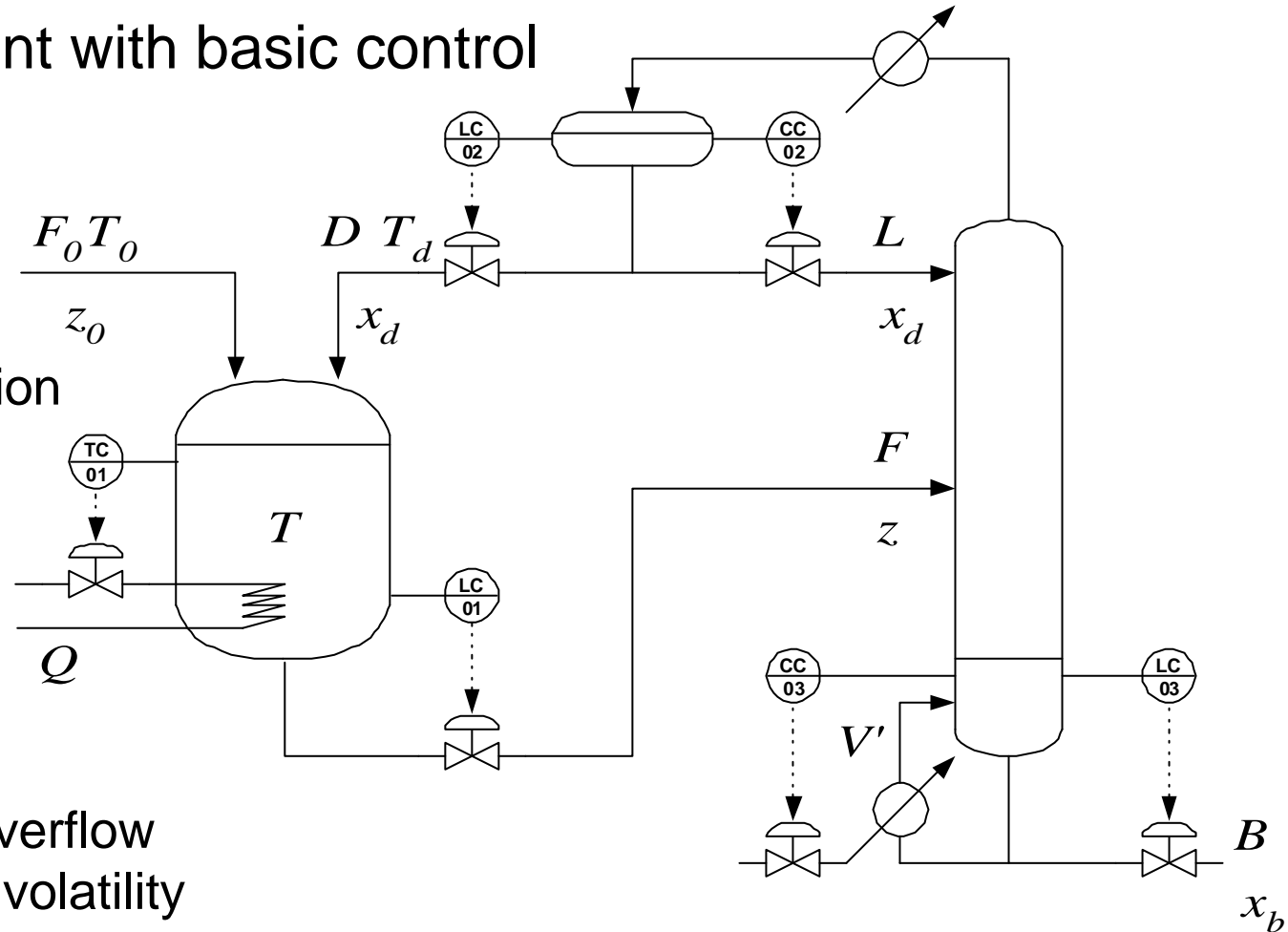
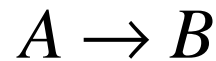
- Problem
  - How to compute this transformation matrix?
- Options
  - Physical based lumping
  - Gramian based input output balancing transformations
  - Proper orthogonal decomposition
- Properties
  - Reduces the number of differential equations
    - Linear control problems are reduced with n-cubed
  - Increases the complexity of the model
    - Effort numerical integration will not be reduced if structure was exploited by the solver



## Dynamics of plant with basic control

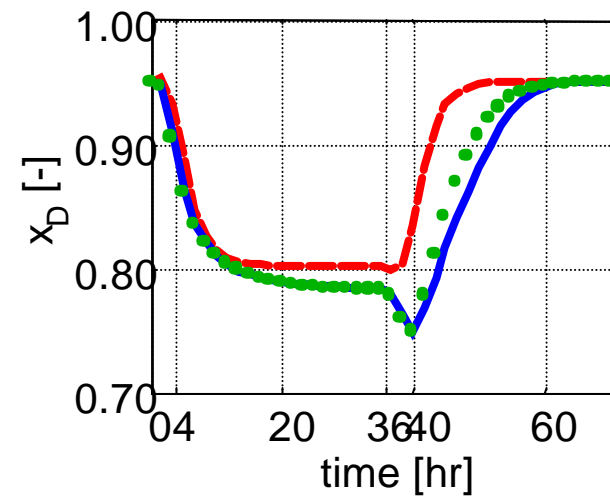
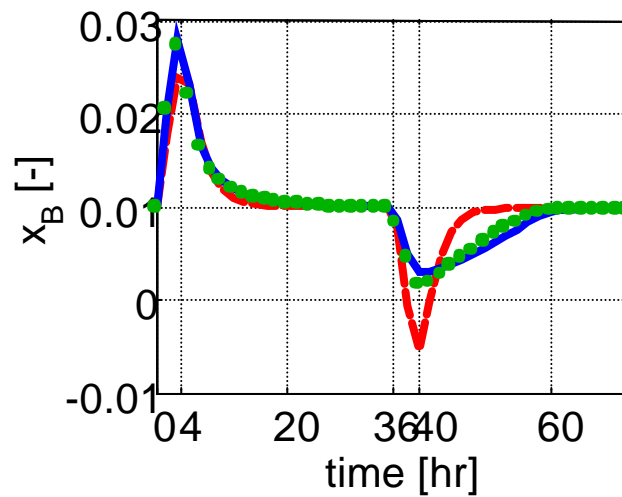
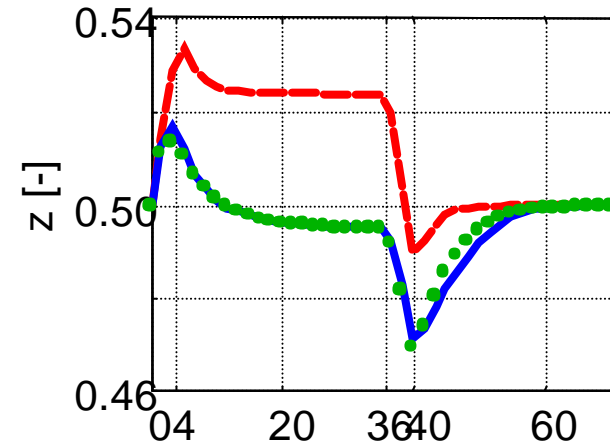
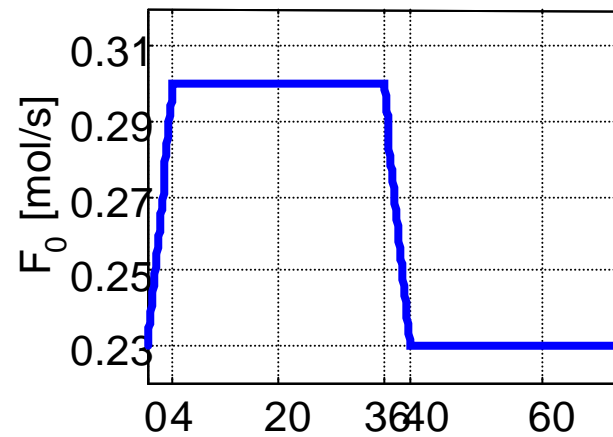
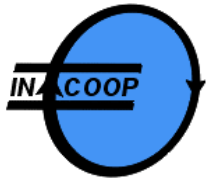
Reactor:

- exothermic reaction

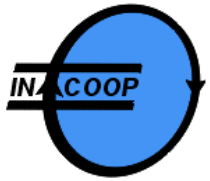


Column:

- constant molar overflow
- constant relative volatility
- 41 trays



legend: original 45<sup>th</sup> order, linearized 45<sup>th</sup> order, reduced 4<sup>th</sup> order.

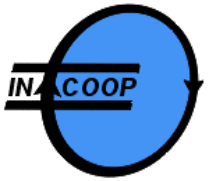


Starting point: Representative trajectory for given  $x_0$  and  $u(t)$

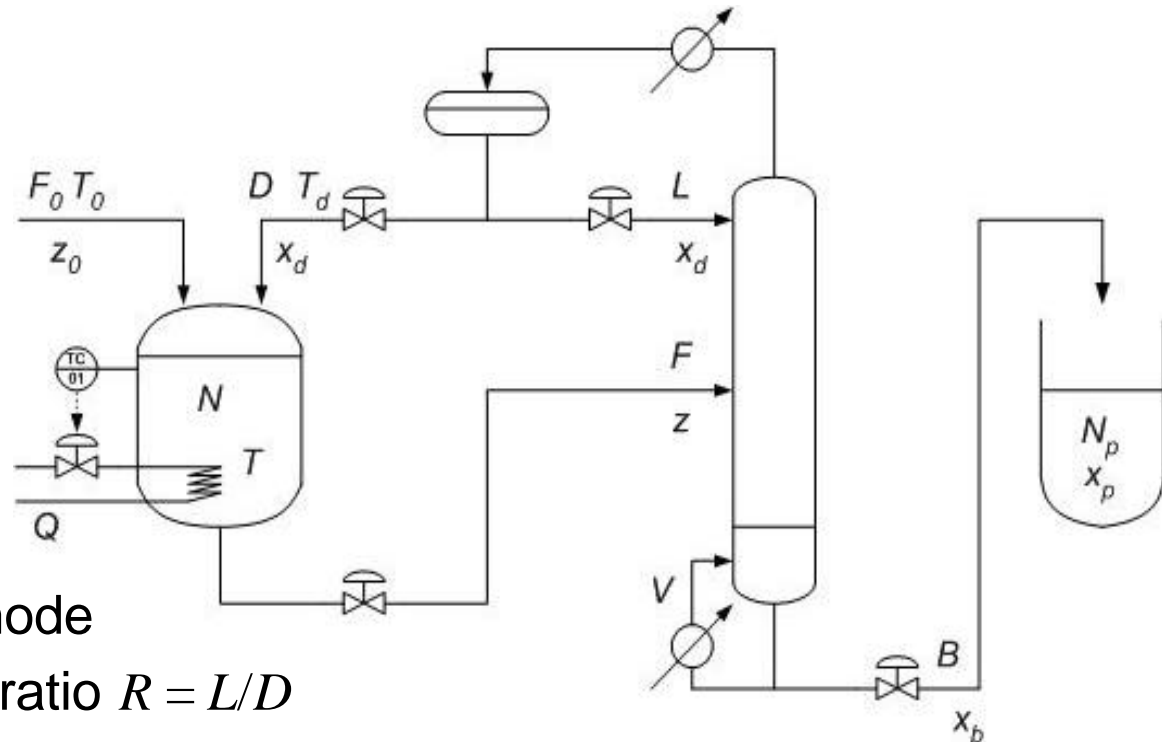
1. Uniformly sample trajectory: *snapshot matrix*  $X = [\Delta x(t_1), \Delta x(t_2), \dots, \Delta x(t_p)]$   
with  $x(t_k) - x^* = \Delta x(t_k)$

2. Singular value decomposition of  $X$  yields basis  $U = [d_1, d_2, \dots, d_p]$

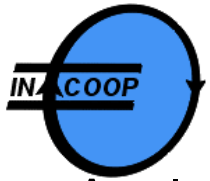
3. a) Select  $p_1 \ll p$  *left singular* vectors of  $X$   
⇒ associated with largest singular values ⇒ capture dominant dynamics  
⇒ corresponds to *truncation*
- b) Use all  $p$  singular vectors of  $X$  as basis  
⇒ can apply *residualization*



## Test plant



- Operated in semi-batch mode
- degree of freedom: reflux ratio  $R = L/D$
- objective: minimize operation time  $t_f$
- endpoint constraints
  - fixed amount of product  $N_p(t_f) = 2000$  mol
  - product composition  $x_p(t_f) = 0.01$
  - path constraint
  - reactor hold-up  $350 \text{ mol} \leq N(t) \leq 600 \text{ mol}$

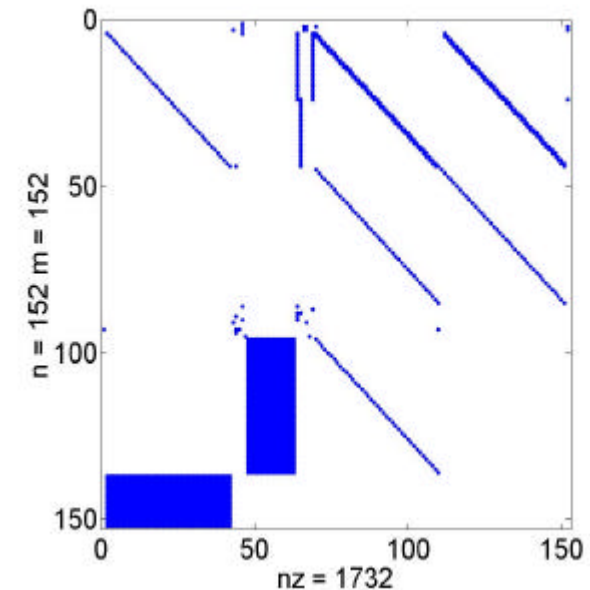
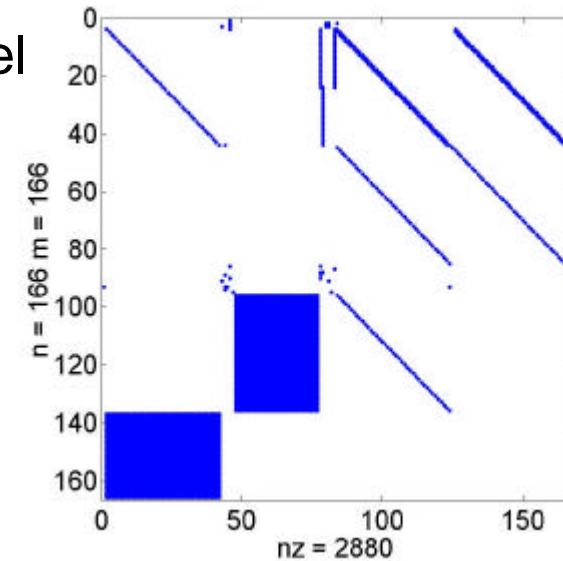


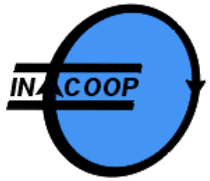
# Solution with truncated model (I)

- Apply projection and truncation to column model
- Original column model: 41 trays = states
- 5 levels of reduction:  
 $n_z = \{30, 20, 18, 16, 8\}$

	model order	iterations	integrations	obj. fun. value	CPU time [s]
nominal	41	31	73	8918.618	169.7
truncation	30	31	73	8918.622	758.1
	20	30	68	8921.933	562.4
	18	27	54	8889.999	397.6
	16	25	64	8958.987	317.5
	8	problem infeasible			

- Projection partly destroys sparsity  
⇒ strongly increased CPU time
- Projection deteriorates optimality



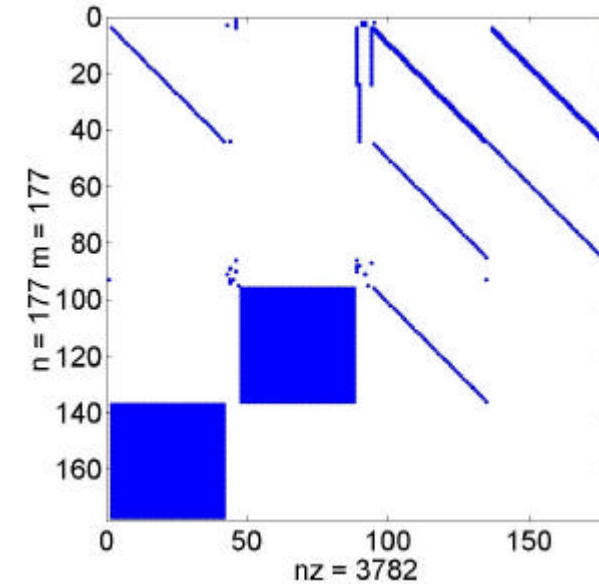


# Solution with residualized model

- Apply projection and residualization to column model
- Original column model: 41 trays = states
- 3 levels of reduction:

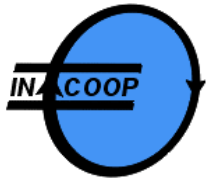
$$n_z = \{30, 16, 8\}$$

	model order	iterations	integrations	obj. fun. value	CPU time [s]
nominal	41	31	73	8918.618	169.7
residualization	30	31	73	8918.618	975.6
	16	32	77	8918.614	1083.2
	8	31	74	8916.406	1025.8

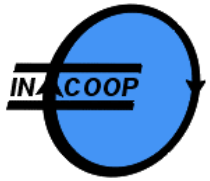


- Solution almost identical to nominal case
- Matrix fill-up independent of reduction level  
⇒ CPU time in the same order of magnitude, but much higher as nominal

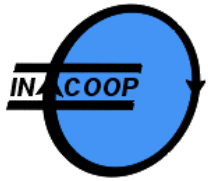




- Problem
  - Need state to initialize model
  - Given measured data produce state-estimate
- Solution
  - Least squares horizon estimation
  - LTV approximation instead of true nonlinear
  - Single step LTV gives Extended Kalman Filter (EKF)
- Features:
  - Multi-rate measurements
  - Constraints on process variables
  - Delayed measurements
  - Primitive line-search

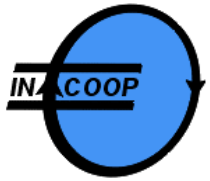


- Problem
  - Large number of parameters  $> nx+H*nx$
  - Ill-conditioning of estimation problem
  - Tuning estimation function difficult
- Solution
  - Select only relevant input/output behaviour
  - Reduce number of differential variables
  - Uncertain feeds/energy flows to measured process variables
  - I/O balanced model-reduction
- Properties
  - Well conditioned small problem
  - Physical interpretation in dominant modes
  - Online feasible / reliable from certain number of states downwards

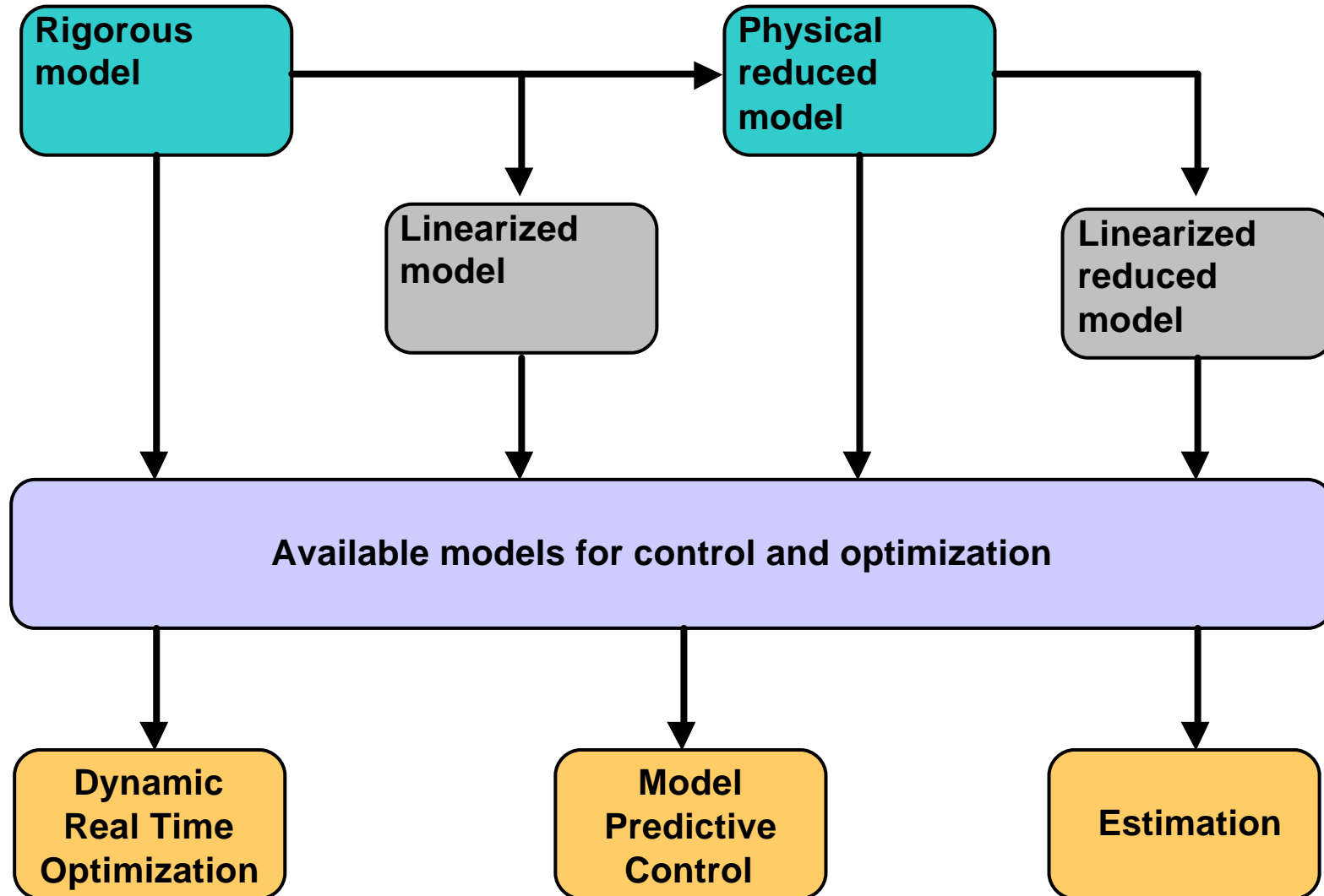


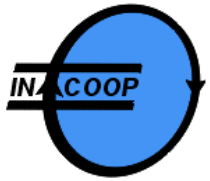
<ul style="list-style-type: none"><li>• Compute Jacobian of the model</li></ul>	$\dot{x} = f(x, y, u)$ $0 = g(x, y, u)$
<ul style="list-style-type: none"><li>• Derive linear model</li></ul>	$\Delta\dot{x} = A\Delta x + B\Delta u$ $\Delta y = C\Delta x + D\Delta u$
<ul style="list-style-type: none"><li>• First reduction linear model with fixed projection (<i>e.g. remove connectivity</i>)</li></ul>	$\Delta\dot{z} = \tilde{A}\Delta z + \tilde{B}\Delta u$ $\Delta y = \tilde{C}\Delta z + D\Delta u$
<ul style="list-style-type: none"><li>• Second reduction on reduced linear model by balanced truncation (online)</li></ul>	$\Delta\dot{z}_b = \hat{A}\Delta z_b + \hat{B}\Delta u$ $\Delta y = \hat{C}\Delta z_b + D\Delta u$

Significant computational savings obtained due to  $n^3$  effect in control computations

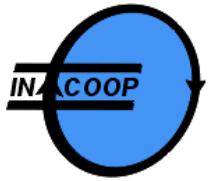


# Available models for control and optimization **TU Delft**

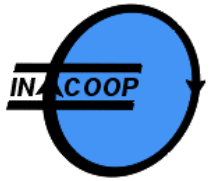




- Is it possible to reduce the model while retaining structure?
- Can one reduce the number of equation significantly?
- Can the application aspect be directly considered in the reduction procedure?



- Model synthesis: systematic approach needed
- Model reduction for ChE DAE systems: mixed results  
*Reducing number of equations helps better than shifting the balance between ODE's and AE's in DAE problems.  
If algorithms exploit sparsity, order reduction is less effective.*
- Modelling and model complexity reduction for integrated d-optimisation & control largely open  
Key issues:
  - *combination of fundamental and empirical model components*
  - *physical based lumping (species, phases, reactions)*
  - *model complexity reduction*
  - *real time adaptation of structure of reduced models*
  - *consistency of reduced models for various tasks*
  - *closed loop model validation*



**INCOOP Workshop  
Düsseldorf, 23-24 January, 2003**