

## A new retuning approach for DoA reference tracking improvement <sup>\*</sup>

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**Abstract:** In this paper, a retuning strategy for a controller is proposed in order to improve the reference BIS tracking in patients, by means of simultaneous administration of *propofol* and of *remifentanyl*, in the presence of model uncertainties. This strategy proves to be useful as is shown by simulations.

Keywords: Automatic control; DoA; Anesthesia.

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### 1. INTRODUCTION

One of the most important concerns of the anesthetists during surgery is the administration of the right combination of drugs in order to achieve a desired depth of anesthesia (DoA). The DoA consists of two components, the hypnosis and the analgesia. The study presented in this paper concerns the case where hypnosis and analgesia are achieved, respectively, by the administration of *propofol* and of *remifentanyl*. Moreover, following several studies (Tirén et al. [2005], Grindstaff and Tobias [2004], Ekman et al. [2004], Wodey et al. [2005], Whyte and Booker [2003]) and clinical practice, the level of DoA is measured by means of the bispectral index (BIS). This index is a single dimensionless number, which is computed from the electroencephalogram (EEG) and ranges from 0 (equivalent to EEG silence) to 100 (equivalent to fully awake and alert). According to medical practice a BIS value between 40 and 60 corresponds to an appropriate DoA level for general anesthesia.

After an adequate model for the BIS response of a patient to the administration of *propofol* and *remifentanyl* is identified, the desired BIS value may be tracked by the automatic controller developed in Nogueira et al. [2014] (see also Nogueira et al. [2012]). However, in the presence of

uncertainties, due to errors in modeling and identification procedures, the BIS obtained may be different from the desired one. In this work, we present a controller retuning strategy in order to overcome this problem. The proposed retuning strategy improves the BIS reference tracking as illustrated by simulations.

### 2. MODEL DESCRIPTION

The patient BIS response to the administration of *propofol* and of *remifentanyl* is commonly modeled as a high order pharmacokinetic/pharmacodynamic (PK/PD) Wiener model, which is constituted by a dynamic linear part based on the relevant patient characteristics (see Bailey and Haddad [2005], Schnider et al. [1998], Marsh et al. [1991], Minto et al. [1997]) and by a nonlinear static part (see Minto et al. [2000]). However, a new Wiener model (parameter parsimonious Wiener model) with a reduced number of parameters describing the joint effect of *propofol* and of *remifentanyl* has been introduced in Silva et al. [2010].

In the parameter parsimonious model (PPM) the relation between the *propofol* and *remifentanyl* dosages and the corresponding effect concentrations ( $c_e^p$  and  $c_e^r$ ) are modeled by the transfer functions:

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$$H^p(s) = \frac{k_1 k_2 k_3 \alpha^3}{(k_1 \alpha + s)(k_2 \alpha + s)(k_3 \alpha + s)} u^p(s), \quad (1)$$

$$H^r(s) = \frac{l_1 l_2 l_3 \eta^3}{(l_1 \eta + s)(l_2 \eta + s)(l_3 \eta + s)} u^r(s), \quad (2)$$

respectively, where  $\alpha$  and  $\eta$  are patient dependent parameters, without any physiological meaning. The corresponding BIS level,  $z(t)$ , usually given by the generalized Hill equation Minto et al. [2000], is approximated in Silva et al. [2010] by the nonlinear equation:

$$z(t) = \frac{z_0}{1 + (U(t))^\gamma}, \quad (3)$$

where  $U(t) = \mu U^p + U^r$ , and  $\mu$  and  $\gamma$  are patient dependent parameters, without any physiological meaning,  $z_0$  is the BIS level at zero concentration, and  $U^p$  and  $U^r$  respectively denote the potencies of *propofol* and *remifentanyl*, which are obtained by normalizing the effect concentrations with respect to the concentrations that produce half the maximal effect when the drug acts isolated (denoted by  $EC_{50}^p$  and  $EC_{50}^r$ , respectively), i.e.:

$$U^p = \frac{c_e^p}{EC_{50}^p} \text{ and } U^r = \frac{c_e^r}{EC_{50}^r}. \quad (4)$$

The parameters  $EC_{50}^p$  and  $EC_{50}^r$  are taken to be fixed, namely  $EC_{50}^p = 10 \text{ mg/ml}$  and  $EC_{50}^r = 0.01 \text{ mg/ml}$ . These values were obtained in the work developed in Mendonça et al. [2012], to which we refer for further explanation.

### 3. DEPTH OF ANESTHESIA CONTROLLER

In the work developed in Nogueira et al. [2014] (see also Nogueira et al. [2012]), a nonlinear controller was presented in order to track a desired reference value for the BIS level, by means of simultaneous administration of *propofol* and of *remifentanyl*. This controller results from a combination of a linear control law with a positivity constraint for the drug doses and is based on the state space realizations  $\Sigma^p = (A^p, B^p, C^p)$  of the transfer function  $H^p(s)$  and  $\Sigma^r = (A^r, B^r, C^r)$  of  $H^r(s)$ . The matrices of such realizations are as follows:

$$\begin{aligned} A^p &= \begin{bmatrix} -10\alpha & 0 & 0 \\ 9\alpha & -9\alpha & 0 \\ 0 & \alpha & -\alpha \end{bmatrix}, \\ B^p &= \begin{bmatrix} 10\alpha \\ 0 \\ 0 \end{bmatrix}, \\ C^p &= [0 \ 0 \ 1], \\ A^r &= \begin{bmatrix} -3\eta & 0 & 0 \\ 2\eta & -2\eta & 0 \\ 0 & \eta & -\eta \end{bmatrix}, \\ B^r &= \begin{bmatrix} 3\eta \\ 0 \\ 0 \end{bmatrix}, \\ C^r &= [0 \ 0 \ 1]. \end{aligned} \quad (5)$$

Further, the states of  $\Sigma^p$  and of  $\Sigma^r$  are respectively denoted by  $x^p$  and  $x^r$ .

The controller is then defined by:

$$u(t) = \begin{bmatrix} u^p(t) \\ u^r(t) \end{bmatrix} = \begin{bmatrix} \max(0, \tilde{u}^p(t)) \\ \max(0, \tilde{u}^r(t)) \end{bmatrix}, \quad (6)$$

where  $u^p$  is the input of *propofol* and  $u^r$  is the input of *remifentanyl*, with:

$$\begin{bmatrix} \tilde{u}^p \\ \tilde{u}^r \end{bmatrix} = E(-K A x + \lambda(M^* - K x)), \quad (7)$$

where

$$x = \begin{bmatrix} x^p \\ x^r \end{bmatrix}, \quad (8)$$

$$A = \begin{bmatrix} A^p & 0 \\ 0 & A^r \end{bmatrix}, \quad (9)$$

$$E = \begin{bmatrix} \rho \\ 1 \end{bmatrix} \frac{1}{\alpha\rho + 300\eta}, \quad (10)$$

$$M^* = \frac{3(0.1\rho + 100)}{0.1\mu\rho + 100} \left( \frac{z_0}{z^*} - 1 \right)^{\frac{1}{\gamma}}, \quad (11)$$

$$K = [0.1 \ 0.1 \ 0.1 \ 100 \ 100 \ 100], \quad (12)$$

$z^*$  is the desired BIS level, and  $\lambda$  and  $\rho$  are positive design parameters that do not affect the tracked reference value and can be chosen according to clinical criteria. The parameter  $\lambda$  influences the convergence speed to the desired reference value and the parameter  $\rho$  can be interpreted as the proportion between the doses of *propofol* and *remifentanyl*.

For more details about this controller and its tracking properties, the reader is referred to Nogueira et al. [2014] or to Nogueira et al. [2012].

#### 4. RETUNING STRATEGY FOR DOA CONTROL

In this section a strategy is presented to retune the controller described in Section 3 in order to overcome the problems raised by uncertainty in the BIS patient modeling process. The idea is to change the reference value for the parameter  $M^*$  in the control law (7) according to the response of the patient when the controller is applied. For this purpose, we assume that the uncertainties in the model only occur in its linear part and in the parameter  $\mu$ , the parameter  $\gamma$  of the Hill equation (3) is considered to be known. A simple procedure to identify the parameter  $\gamma$  can be found in the work developed in Nogueira et al. [2013].

In the sequel, we denote by  $M_{model}^{ref}$  the target value used in the control law applied to the PPM used to describe a patient in order to achieve a certain reference value for the BIS,  $U_{model}(t)$  denoted the theoretical potency  $U(t)$  obtained for the PPM and  $U_{patient}(t)$  denotes the potency  $U(t)$  obtained for a real patient.

It follows from what has been presented in Nogueira et al. [2014], and summarized in the previous section, that when, in the controller (7), the parameter  $M^*$  is set to:

$$M^* = M_{model}^{ref} = \frac{3(0.1\rho + 100)}{0.1\mu\rho + 100} \left( \frac{z_0}{z^*} - 1 \right)^{\frac{1}{\gamma}}, \quad (13)$$

the desired BIS value  $z^*$  is achieved to the corresponding PPM. This means that the potency  $U_{model}(t)$  converges to a value

$$U^* = \gamma \sqrt{\frac{z_0}{z^*} - 1} \quad (14)$$

$$= \tau M_{model}^{ref}, \quad (15)$$

with  $\tau = \frac{0.1\mu\rho+100}{3(0.1\rho+100)}$ .

However, when the controller is tuned with the parameter  $M^* = M_{model}^{ref}$  as in (13), the BIS level obtained in a real patient will be equal to a certain value  $\bar{z}$  instead of the desired one,  $z^*$ . This means that  $U_{patient}(t)$  converges to a value

$$\bar{U} = \gamma \sqrt{\frac{z_0}{\bar{z}} - 1}. \quad (16)$$

The retuning strategy presented here is based on the assumption that the patient is correctly modeled by a PPM. Moreover it is assumed that the misfit in the achieved BIS values is due to the fact that the actual patient PPM differs from the initially considered one. In this case, the same type of relationship exists as for the original PPM between the steady state value of  $U(t)$  and the value of  $M^*$  taken in the control law (7). I.e., setting  $M^* = \bar{M}$  and applying the corresponding control law to the patient yields a steady state value of  $U(t)$

$$\bar{U} = \bar{\tau} \bar{M}, \quad (17)$$

for an adequate value of  $\bar{\tau}$ . Since  $\bar{M}$  is known, the value of  $\bar{\tau}$  can be computed by letting the system settle down and computing  $\bar{U}$ . In particular, if ones observes that setting  $M^* = M_{mod}^{ref}$  yields a state  $U^{**}$  ( $\neq U^*$ ) for  $U(t)$  one can conclude that

$$\bar{\tau} = \frac{U^{**}}{M_{mod}^{ref}}. \quad (18)$$

This means that, in order to track the BIS reference value  $z^*$ , or equivalently in order to achieve the steady state value  $U^*$  for  $U(t)$ , the adequate value for  $M^*$  in (7) should be given by:

$$M^* = \frac{U^*}{\bar{\tau}} \Leftrightarrow \quad (19)$$

$$M^* = \frac{U^*}{U^{**}} M_{mod}^{ref}. \quad (20)$$

Therefore an improvement of the reference tracking performance can be obtained by means of the following strategy:

Given a PPM for a patient:

- (1) Compute the value  $M^* = M_{mod}^{ref}$  as in (11) according to the PPM parameters.
- (2) Compute the theoretical steady state value  $U^*$  of  $U(t)$  according to equation (14).
- (3) Apply the corresponding control law (7) to deliver the adequate doses of *propofol* and *remifentanyl*.
- (4) Observe the patient response, read out the BIS steady state value  $z^{**}$  and compute the corresponding steady state value  $U^{**}$  of the combined potency  $U(t)$ .
- (5) Retune the value of  $M^*$  in (7) according to the equation (20).

#### 5. SIMULATIONS

In this section, the performance of the retuning strategy for the improvement of the performance of the controller (7) is illustrated by simulations. For this purpose, the control law is applied to a simulated patient that was set up based on the data of a real patient, a woman, with 68 years of age, a height of 158 cm, and 113 Kg who was subject to general anesthesia under *propofol* and *remifentanyl* administration during a breast surgery. The DoA was monitored by the BIS and was manually controlled around clinically accepted values by the anesthetist. Alaris GH pumps were used for both *propofol* and *remifentanyl*. Infusion rates, BIS values and other physiological variables were acquired every five seconds (Mendonça et al. [2012]).

For this patient, a PK/PD Wiener model (other than the PPM) was obtained as follows. The linear part was modeled according to Marsh et al. [1991], Minto et al. [1997], and Schnider et al. [1998] based on the relevant patient characteristics. The corresponding model is summarized in equation (1) of Ionescu et al. [2011], which was

used here with age = 68, height = 158 cm and weight = 113 Kg. The nonlinear part was taken to coincide with the generalized Hill equation (3) and the corresponding parameters  $\gamma$  and  $\mu$  were identified in Mendonça et al. [2012] from the surgery data, being given by:  $\gamma = 1.09$  and  $\mu = 2.40$ .

In order to test the proposed control retuning strategy, the controller is first tuned assuming that the simulated patient is modeled by the parsimonious parameter Wiener model of Silva et al. [2010], with parameters  $\alpha$ ,  $\eta$ , and  $\gamma$  identified as in Mendonça et al. [2012]. These parameters were made available to us by the authors in a private communication and are given by  $\alpha = 0.0687$ ,  $\eta = 4.5413$ , and  $\gamma = 1.09$ . In order to increase the misfit between the theoretical model, PPM, and the simulated patient model, instead of the value  $\mu = 2.40$ , identified for the patient, another value for  $\mu$  is chosen in the PPM, namely  $\mu = 1.79$ . This value is the average of the values for  $\mu$  taken from a bank of identified values for eighteen real patients obtained in the work developed in Mendonça et al. [2012]

Figure 1 shows the BIS response of the patient using the controller (7) without applying the retuning strategy. In this case, the BIS response of the patient converged to 67 instead for the desired reference value,  $z^* = 50$ , i.e., the BIS is affected by an error of 34%.

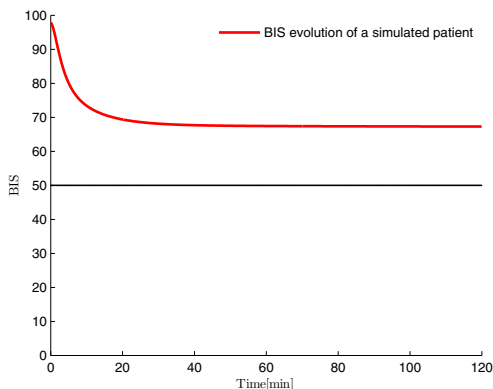


Fig. 1. BIS evolution of a simulated patient without applying the retuning strategy. The desired BIS level is set to be 50.

The illustration of the BIS response of the patient with the retuning strategy is presented in Figures 2 and 3. In Fig. 2 the new reference  $M^*$  was computed at time  $t_1 = 20 \text{ min}$  (when steady state was almost achieved), improving the BIS response of this patient, which converged to 48, value quite close to the desired one. The error of 4%, occurred in this case, would be smaller if the retuning happened later in steady state. However, another retuning may be made, as shown in Fig. 3, where a second retuning occurred at the instant  $t_2 = 60 \text{ min}$  (when the steady state was achieved), which led the BIS response to converge to the desired value  $z^* = 50$ .

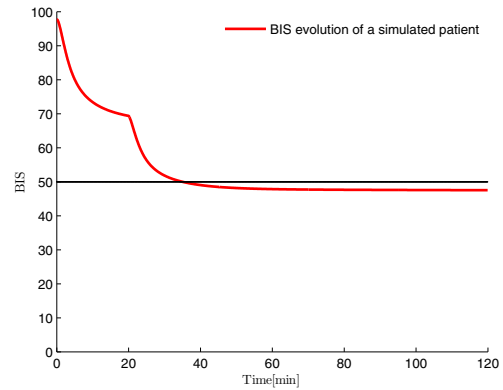


Fig. 2. BIS evolution of a patient modeled by a PK/PD model with a retune strategy applied at time  $t = 20 \text{ min}$ . The desired BIS level is set to be 50.

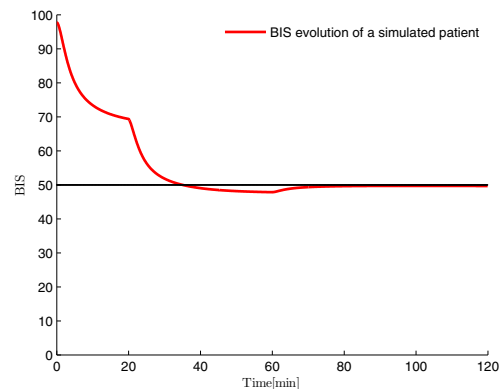


Fig. 3. BIS evolution of a patient modeled by a PK/PD model with a retune strategy applied at time instants  $t_1 = 20 \text{ min}$  and  $t_2 = 60 \text{ min}$ . The desired BIS level is set to be 50.

## 6. EPILOGUE

In this paper, a controller retuning strategy was proposed in order to improve the BIS reference tracking in patients, by means of simultaneous administration of *propofol* and of *remifentanyl*, in the presence of model uncertainties. For this purpose, the patient is simulated by the PK/PD Wiener model proposed in Marsh et al. [1991], Minto et al. [1997], and Schnider et al. [1998], while the controller is tuned for a PPM. Assuming that the misfit in the patient response is due to the existence of errors in the parameters of the PPM, a controller retuning strategy is obtained that improves the reference tracking, as has been shown in the presented simulations.

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